

OCRWM

## DESIGN CALCULATION OR ANALYSIS COVER SHEET

1. QA: QA

2. Page 1

3. System

DRY TRANSFER FACILITY

4. Document Identifier

110-SYC-SY00-00300-000-00A

5. Title

DRY TRANSFER FACILITY SEISMIC ANALYSIS

6. Group

CIVIL/STRUCTURAL/ARCHITECTURAL

7. Document Status Designation

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8. Notes/Comments

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**1) ECN-001, DATED 08/29/2005**

## Attachments

Total Number of Pages

1. GTSTRUDL Output using fixed base boundary condition (CD-ROM)

92

2. GTSTRUDL Output using lower bound 35 soil springs (CD-ROM)

103

3. GTSTRUDL Output using median 35 soil springs (CD-ROM)

103

4. GTSTRUDL Output using upper bound 35 soil springs (CD-ROM)

103

5. GTSTRUDL Output using lower bound 110 soil springs (CD-ROM)

103

6. GTSTRUDL Output using median 110 soil springs (CD-ROM)

103

7. GTSTRUDL Output using upper bound 110 soil springs (CD-ROM)

103

8. Dry Transfer Facility Wall Elevations including Beam Stick Model Joints and Elements I.D.

32

9. Dry Transfer Facility General Arrangement

1

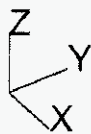
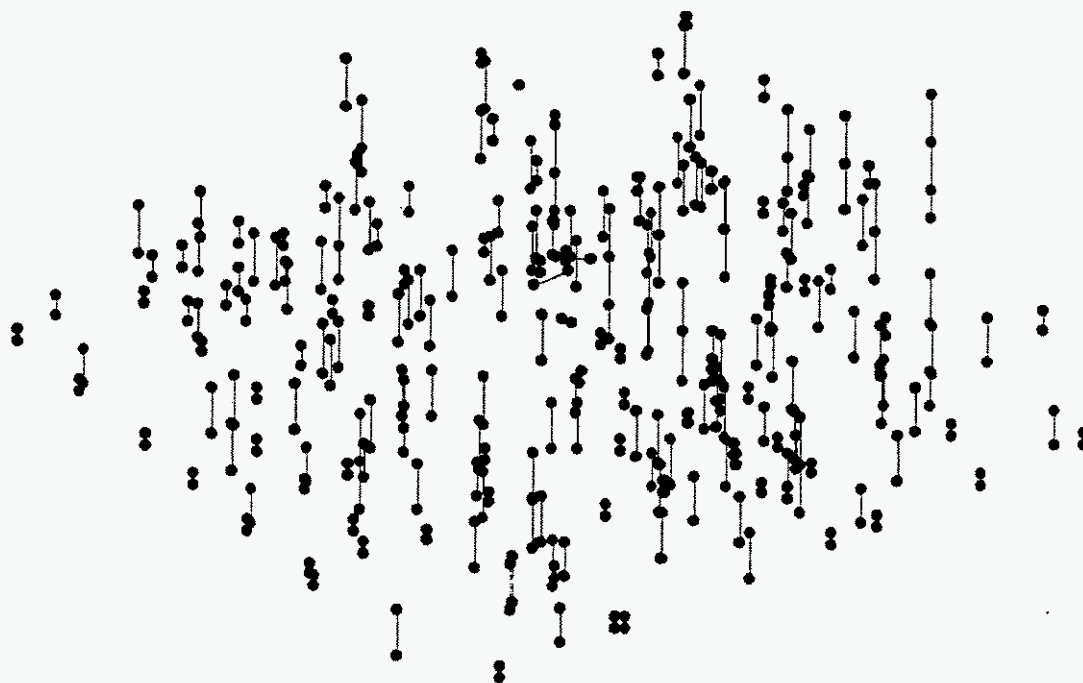
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## **CONTENTS**

	<b>Page</b>
1. PURPOSE .....	5
2. METHOD .....	5
3. QUALITY ASSURANCE .....	5
4. USE OF SOFTWARE .....	5
5. INPUTS .....	6
6. ASSUMPTIONS .....	6
7. CALCULATIONS .....	6
8. RESULTS .....	25
9. REFERENCES .....	25
10. ATTACHMENTS .....	26

## FIGURES

### 3-D View of DTF Beam Element Stick Model



## **TABLES**

**N/A**

## 1. PURPOSE

The purpose of this calculation is to perform a dynamic and static analysis on the Dry Transfer Facility, and to determine the response spectra seismic forces for the design basis ground motions. The resulting seismic forces and accelerations will be used in a subsequent calculation to complete preliminary design of the concrete shear walls, diaphragms, and basemat.

## 2. METHOD

The Cartesian coordinate origin (0,0,0) for the Dry Transfer Facility is located at the intersection of column lines 1.0 and R.0, at Elevation 0'-0" (Ref. Attachment 9, DTF General Arrangement 110-P1K-WHS0-00102-000-00B). The positive X-axis extends from the origin toward column line 13.0 along column line R.0. The positive Y-axis extends from the origin toward column line A.0 along column line 1.0. The positive Z-axis extends vertically upward from the origin.

A three-dimensional stick model (See Figure on Page 3) was created incorporating the mass and stiffness properties calculated in Design Calculation 110-SYC-SY00-00200-000-00A. The mass for each floor was lumped at a dedicated node located at the coordinates for the center of mass. "Dummy" elements with zero stiffness were used to provide continuity between the center of mass and the center of rigidity at each primary floor level; elevations 0, 32, 66, 100, and 107ft. Rigid solids or "links" were used to simulate a rigid floor diaphragm. The center of rigidity was used as the master node for the rigid links. All other nodes lying on the same floor elevation were slaved to the master node. Attachment 8 shows the wall elevations with the GTSTRUDL beam elements and joints labeled for the Dry Transfer Facility.

A support spring with six degrees of freedom was placed at the center of rigidity (GTSTRUDL node 100) of the basemat. Seven analysis runs were performed using six bounding support spring conditions, as well as one fixed base solution. Three springs were calculated, each at two different soil depths (35 feet and 110 feet), yielding six support spring conditions. The naming convention for the six support spring constants used are; lower bound 35, median 35, upper bound 35 (highest stiffness), lower bound 110 (lowest stiffness), median 110, upper bound 110. These bounding spring constants were computed in Design Calculation 110-CYC-CY00-00100-000-00A using the requirements of ASCE 4-98 for frequency independent soil springs. Reference the preceding calculation for a complete description of the soil spring methodology. A modal analysis was performed after specifying the boundary conditions. A response spectrum analysis was then performed for each boundary condition using the seismic design spectra determined for the surface facilities area (Ref. DTN: MO0402SDSTMHIS.004, "SEISMIC DESIGN SPECTRA AND TIME HISTORIES FOR THE SURFACE FACILITIES AREA (POINT D/E) AT 5E-4 ANNUAL EXCEEDANCE FREQUENCY," Silva, W.J.). The response spectra accelerations for 20% critical damping were used for the first three modes and 7% critical damping values were used for the remaining modes.

The forces and accelerations will be determined for each of the three global directions; HX, HY, and VZ. HX and HY represent both orthogonal horizontal directions and VZ represents the vertical direction. The modal contributions are combined using the NRC "Ten Percent Method." After combining the global modes, pseudo-static loadings for each global direction are created using the dynamic results. Pseudo-static loads create usable static results computed using the dynamic results. These three independent pseudo-static load cases are then combined using the SRSS method. A stiffness analysis is also performed within GTSTRUDL for the dead load case. The dead load case is the weight (mass) used in determining the seismic forces, which is comprised of the structure's self weight plus 25% of the applied live load.

## 3. QUALITY ASSURANCE

This calculation is for the Dry Transfer Facility, which is designated as an important to safety structure by the *Q-List*, TDR-MGR-RL-000005 (BSC 2003). Therefore the requirements of the *Quality Assurance Requirements and Description* (DOE 2003) are applicable to this calculation.

## 4. USE OF SOFTWARE

Microsoft Excel 97 SR-2 was used to build the GTSTRUDL input file. The qualified finite element computer code GTSTRUDL version 26, which is identified with the Software Tracking Number 10829-26-00, was utilized in this calculation package to perform the dynamic and static analysis on the Dry Transfer Facility.

GTSTRUDL is a commercially available computer code qualified for performing static and dynamic analysis of structural systems, and it is in this capacity that the software is used. GTSTRUDL was not used outside of its range of qualification. The software is operated on a PC system running the Windows 2000 operating system.

## 5. INPUTS

"SEISMIC DESIGN SPECTRA AND TIME HISTORIES FOR THE SURFACE FACILITIES AREA (POINT D/E) AT SE-4 ANNUAL EXCEEDANCE FREQUENCY," Silva, W.J., DTN: MO0402SDSTMHIS.004

Mass and stiffness properties calculated in Design Calculation 110-SYC-SY00-00200-000-00A.

Support spring constants calculated in Design Calculation 110-CYC-CY00-00100-000-00A.

## 6. ASSUMPTIONS

This calculation is based on the output of Design Calculation 110-SYC-SY00-00200-000-00A. It is assumed that the referenced output is bounding and of sufficient accuracy to be used in this calculation.

## 7. CALCULATIONS

This section contains the actual GTSTRUDL input file used for running the seven individual boundary condition cases. The output is given in attachments 1 through 7.

```
STRUDL 'DTF 1' 'RESPONSE SPECTRA ANALYSIS USING SOIL SPRINGS'
$
UNITS      FEET      KIPS      DEGREES
$
JOINT COORDINATES
$ Elev. 0
1      0.0      246.0      15.0      $ Wall Column Line 1-1
2      48.0      247.3      15.0      $ Wall Column Line 3-1
3      89.0      281.5      10.0      $ Wall Column Line 3.5-1
4      123.0      193.8      0.0      $ Wall Column Line 4-1
5      123.0      295.5      8.0      $ Wall Column Line 4-2
6      123.0      398.4      0.0      $ Wall Column Line 4-3
7      147.0      38.9      0.0      $ Wall Column Line 5-1
8      147.0      122.1      0.0      $ Wall Column Line 5-2
9      147.0      192.6      0.0      $ Wall Column Line 5-3
10     147.0      243.5      0.0      $ Wall Column Line 5-4
11     147.0      295.0      0.0      $ Wall Column Line 5-5
12     147.0      346.5      0.0      $ Wall Column Line 5-6
13     147.0      442.5      8.0      $ Wall Column Line 5-7
14     171.0      80.6      0.0      $ Wall Column Line 6-1
15     195.0      139.6      0.0      $ Wall Column Line 7-1
16     195.0      237.0      0.0      $ Wall Column Line 7-2
17     195.0      412.0      0.0      $ Wall Column Line 7-3
18     207.0      453.9      0.0      $ Wall Column Line 7.5-1
19     225.0      388.0      8.0      $ Wall Column Line 8.3-1
20     259.0      216.5      8.0      $ Wall Column Line 9-1
21     259.0      386.0      0.0      $ Wall Column Line 9-2
22     295.0      122.1      8.0      $ Wall Column Line 10-1
23     295.0      289.0      8.0      $ Wall Column Line 10-2
24     295.0      386.0      0.0      $ Wall Column Line 10-3
25     277.0      93.1      0.0      $ Wall Column Line 9.5-1
26     344.0      133.5      0.0      $ Wall Column Line 11-1
27     344.0      211.0      8.0      $ Wall Column Line 11-2
28     344.0      289.0      8.0      $ Wall Column Line 11-3
29     344.0      373.0      0.0      $ Wall Column Line 11-4
30     344.0      446.9      0.0      $ Wall Column Line 11-5
31     377.0      216.8      0.0      $ Wall Column Line 12-1
32     377.0      289.0      8.0      $ Wall Column Line 12-2
33     377.0      373.0      0.0      $ Wall Column Line 12-3
34     442.0      78.1      8.0      $ Wall Column Line 13-1
35     442.0      210.8      0.0      $ Wall Column Line 13-2
36     442.0      288.8      8.0      $ Wall Column Line 13-3
37     442.0      425.9      8.0      $ Wall Column Line 13-4
```

\$				
38	221.0	492.0	13.0	\$ Wall Column Line A-1
39	171.0	466.0	0.0	\$ Wall Column Line B-1
40	184.0	414.0	13.0	\$ Wall Column Line D-1
41	95.0	402.0	0.0	\$ Wall Column Line D.5-1
42	119.9	388.0	0.0	\$ Wall Column Line E-1
43	369.1	388.0	8.0	\$ Wall Column Line E-2
44	114.3	362.0	0.0	\$ Wall Column Line F-1
45	246.6	362.0	0.0	\$ Wall Column Line F-2
46	114.3	336.0	0.0	\$ Wall Column Line G-1
47	269.5	336.0	0.0	\$ Wall Column Line G-2
48	210.0	274.0	8.0	\$ Wall Column Line J-5
49	119.9	310.0	0.0	\$ Wall Column Line H-1
50	270.6	310.0	0.0	\$ Wall Column Line H-2
51	119.9	283.5	0.0	\$ Wall Column Line H.75-1
52	305.5	274.0	0.0	\$ Wall Column Line J-1
53	388.9	274.0	8.0	\$ Wall Column Line J-2
54	114.3	257.5	0.0	\$ Wall Column Line J.4-1
55	114.3	231.0	0.0	\$ Wall Column Line J.9-1
56	305.5	226.0	0.0	\$ Wall Column Line K-1
57	339.0	226.0	0.0	\$ Wall Column Line K-2
58	409.5	226.0	0.0	\$ Wall Column Line K-3
59	119.9	204.5	0.0	\$ Wall Column Line K.5-1
60	279.2	204.5	0.0	\$ Wall Column Line K.5-2
61	271.0	192.0	0.0	\$ Wall Column Line K.8-1
62	72.6	180.0	8.0	\$ Wall Column Line L-1
63	396.6	180.0	0.0	\$ Wall Column Line L-2
65	205.0	154.0	0.0	\$ Wall Column Line M-1
66	305.5	154.0	0.0	\$ Wall Column Line M-2
68	56.9	119.0	15.0	\$ Wall Column Line N-1
69	225.5	119.0	0.0	\$ Wall Column Line N-2
70	305.5	119.0	0.0	\$ Wall Column Line N-3
71	388.9	119.0	8.0	\$ Wall Column Line N-4
72	73.6	80.0	8.0	\$ Wall Column Line O-1
73	242.4	80.0	8.0	\$ Wall Column Line O-2
74	388.9	80.0	0.0	\$ Wall Column Line O-3
75	227.1	50.0	8.0	\$ Wall Column Line P-1
76	73.6	0.0	8.0	\$ Wall Column Line R-1
77	242.5	0.0	8.0	\$ Wall Column Line R-2
78	388.9	0.0	0.0	\$ Wall Column Line R-3
79	135.0	136.5	0.0	\$ Wall Column Line 4.5-1
80	147.0	397.8	0.0	\$ Wall Column Line 5-9
81	225.0	290.0	0.0	\$ Wall Column Line 8.3-4
82	410.6	336.0	0.0	\$ Wall Column Line G-3
83	344.0	86.8	0.0	\$ Wall Column Line 11-8
84	384.0	85.3	0.0	\$ Wall Column Line 12.1-1
85	384.0	113.8	0.0	\$ Wall Column Line 12.1-2
86	-17.8	145.0	0.0	\$ Wall Column Line M.3-1
87	69.9	145.0	0.0	\$ Wall Column Line M.3-2
\$				
1000	0.0	31.9	0.0	\$ Wall Column Line 1-a
1001	0.0	99.0	0.0	\$ Wall Column Line 1-b
1002	0.0	160.1	0.0	\$ Wall Column Line 1-c
1003	0.0	220.6	0.0	\$ Wall Column Line 1-d
1004	0.0	339.0	0.0	\$ Wall Column Line 1-e
1005	0.0	454.4	0.0	\$ Wall Column Line 1-f
1006	48.0	90.9	0.0	\$ Wall Column Line 3-a
1007	48.0	117.9	0.0	\$ Wall Column Line 3-b
1008	48.0	160.1	0.0	\$ Wall Column Line 3-c
1009	48.0	223.9	0.0	\$ Wall Column Line 3-d
1010	48.0	336.8	0.0	\$ Wall Column Line 3-e
1011	89.0	164.5	0.0	\$ Wall Column Line 3.5-a
1012	89.0	214.6	0.0	\$ Wall Column Line 3.5-b
1013	89.0	271.4	0.0	\$ Wall Column Line 3.5-c
1014	89.0	319.8	0.0	\$ Wall Column Line 3.5-d
1015	89.0	378.0	0.0	\$ Wall Column Line 3.5-e
1016	123.0	286.0	0.0	\$ Wall Column Line 4-a
1017	123.0	305.0	0.0	\$ Wall Column Line 4-b
1018	147.0	425.5	0.0	\$ Wall Column Line 5-a
1019	147.0	454.0	0.0	\$ Wall Column Line 5-b
1020	225.0	374.8	0.0	\$ Wall Column Line 8.3-a
1021	225.0	401.0	0.0	\$ Wall Column Line 8.3-b
1022	259.0	153.5	0.0	\$ Wall Column Line 9-a
1023	259.0	250.5	0.0	\$ Wall Column Line 9-b
1024	259.0	312.0	0.0	\$ Wall Column Line 9-c
1025	295.0	5.1	0.0	\$ Wall Column Line 10-a
1026	295.0	42.3	0.0	\$ Wall Column Line 10-b
1027	295.0	130.5	0.0	\$ Wall Column Line 10-c
1028	295.0	223.0	0.0	\$ Wall Column Line 10-d
1029	295.0	269.8	0.0	\$ Wall Column Line 10-e
1030	295.0	291.8	0.0	\$ Wall Column Line 10-f
1031	295.0	312.0	0.0	\$ Wall Column Line 10-g
1032	344.0	177.8	0.0	\$ Wall Column Line 11-a
1033	344.0	218.8	0.0	\$ Wall Column Line 11-b
1034	344.0	268.8	0.0	\$ Wall Column Line 11-c
1035	344.0	298.3	0.0	\$ Wall Column Line 11-d

1036	377.0	265.0	0.0	\$ Wall Column Line 12-a
1037	377.0	300.0	0.0	\$ Wall Column Line 12-b
1038	442.0	37.0	0.0	\$ Wall Column Line 13-a
1039	442.0	123.3	0.0	\$ Wall Column Line 13-b
1040	442.0	268.5	0.0	\$ Wall Column Line 13-c
1041	442.0	300.0	0.0	\$ Wall Column Line 13-d
1042	442.0	373.0	0.0	\$ Wall Column Line 13-e
1043	442.0	446.9	0.0	\$ Wall Column Line 13-f
\$				
1044	53.4	492.0	0.0	\$ Wall Column Line A-a
1045	157.6	492.0	0.0	\$ Wall Column Line A-b
1046	334.9	492.0	0.0	\$ Wall Column Line A-c
1047	111.0	414.0	0.0	\$ Wall Column Line D-a
1048	231.5	414.0	0.0	\$ Wall Column Line D-b
1049	288.0	414.0	0.0	\$ Wall Column Line D-c
1050	319.3	388.0	0.0	\$ Wall Column Line E-a
1051	392.0	388.0	0.0	\$ Wall Column Line E-b
1052	201.5	274.0	0.0	\$ Wall Column Line J-a
1053	220.5	274.0	0.0	\$ Wall Column Line J-b
1054	335.0	274.0	0.0	\$ Wall Column Line J-c
1055	388.6	274.0	0.0	\$ Wall Column Line J-d
1056	17.1	180.0	0.0	\$ Wall Column Line L-a
1057	103.5	180.0	0.0	\$ Wall Column Line L-b
1058	1.1	119.0	0.0	\$ Wall Column Line N-a
1059	66.6	119.0	0.0	\$ Wall Column Line N-b
1060	121.9	119.0	0.0	\$ Wall Column Line N-c
1061	378.0	119.0	0.0	\$ Wall Column Line N-d
1062	438.4	119.0	0.0	\$ Wall Column Line N-e
1063	18.4	80.0	0.0	\$ Wall Column Line O-a
1064	77.3	80.0	0.0	\$ Wall Column Line O-b
1065	134.3	80.0	0.0	\$ Wall Column Line O-c
1066	225.9	80.0	0.0	\$ Wall Column Line O-d
1067	305.5	80.0	0.0	\$ Wall Column Line O-e
1068	176.3	50.0	0.0	\$ Wall Column Line P-a
1069	223.8	50.0	0.0	\$ Wall Column Line P-b
1070	274.5	50.0	0.0	\$ Wall Column Line P-c
1071	7.9	0.0	0.0	\$ Wall Column Line R-a
1072	69.1	0.0	0.0	\$ Wall Column Line R-b
1073	134.9	0.0	0.0	\$ Wall Column Line R-c
1074	183.5	0.0	0.0	\$ Wall Column Line R-d
1075	238.5	0.0	0.0	\$ Wall Column Line R-e
1076	305.5	0.0	0.0	\$ Wall Column Line R-f
\$				
\$ Elev. 8, 10, 13 and 15				
\$				
2000	0.0	31.9	15.0	\$ Wall Column Line 1-a
2001	0.0	99.0	15.0	\$ Wall Column Line 1-b
2002	0.0	160.1	15.0	\$ Wall Column Line 1-c
2003	0.0	220.6	15.0	\$ Wall Column Line 1-d
2004	0.0	339.0	15.0	\$ Wall Column Line 1-e
2005	0.0	454.4	15.0	\$ Wall Column Line 1-f
2006	48.0	90.9	15.0	\$ Wall Column Line 3-a
2007	48.0	117.9	15.0	\$ Wall Column Line 3-b
2008	48.0	160.1	15.0	\$ Wall Column Line 3-c
2009	48.0	223.9	15.0	\$ Wall Column Line 3-d
2010	48.0	336.8	15.0	\$ Wall Column Line 3-e
2011	89.0	164.5	10.0	\$ Wall Column Line 3.5-a
2012	89.0	214.6	10.0	\$ Wall Column Line 3.5-b
2013	89.0	271.4	10.0	\$ Wall Column Line 3.5-c
2014	89.0	319.8	10.0	\$ Wall Column Line 3.5-d
2015	89.0	378.0	10.0	\$ Wall Column Line 3.5-e
2016	123.0	286.0	8.0	\$ Wall Column Line 4-a
2017	123.0	305.0	8.0	\$ Wall Column Line 4-b
2018	147.0	425.5	8.0	\$ Wall Column Line 5-a
2019	147.0	454.0	8.0	\$ Wall Column Line 5-b
2020	225.0	374.8	8.0	\$ Wall Column Line 8.3-a
2021	225.0	401.0	8.0	\$ Wall Column Line 8.3-b
2022	259.0	153.5	8.0	\$ Wall Column Line 9-a
2023	259.0	250.5	8.0	\$ Wall Column Line 9-b
2024	259.0	312.0	8.0	\$ Wall Column Line 9-c
2025	295.0	5.1	8.0	\$ Wall Column Line 10-a
2026	295.0	42.3	8.0	\$ Wall Column Line 10-b
2027	295.0	130.5	8.0	\$ Wall Column Line 10-c
2028	295.0	223.0	8.0	\$ Wall Column Line 10-d
2029	295.0	269.8	8.0	\$ Wall Column Line 10-e
2030	295.0	291.8	8.0	\$ Wall Column Line 10-f
2031	295.0	312.0	8.0	\$ Wall Column Line 10-g
2032	344.0	177.8	8.0	\$ Wall Column Line 11-a
2033	344.0	218.8	8.0	\$ Wall Column Line 11-b
2034	344.0	268.8	8.0	\$ Wall Column Line 11-c
2035	344.0	298.3	8.0	\$ Wall Column Line 11-d
2036	377.0	265.0	8.0	\$ Wall Column Line 12-a
2037	377.0	300.0	8.0	\$ Wall Column Line 12-b
2038	442.0	37.0	8.0	\$ Wall Column Line 13-a
2039	442.0	123.3	8.0	\$ Wall Column Line 13-b
2040	442.0	268.5	8.0	\$ Wall Column Line 13-c



2041	442.0	300.0	8.0	\$ Wall Column Line 13-d
2042	442.0	373.0	8.0	\$ Wall Column Line 13-e
2043	442.0	446.9	8.0	\$ Wall Column Line 13-f
\$				
2044	53.4	492.0	13.0	\$ Wall Column Line A-a
2045	157.6	492.0	13.0	\$ Wall Column Line A-b
2046	334.9	492.0	13.0	\$ Wall Column Line A-c
2047	111.0	414.0	13.0	\$ Wall Column Line D-a
2048	231.5	414.0	13.0	\$ Wall Column Line D-b
2049	288.0	414.0	13.0	\$ Wall Column Line D-c
2050	319.3	388.0	8.0	\$ Wall Column Line E-a
2051	392.0	388.0	8.0	\$ Wall Column Line E-b
2052	201.5	274.0	8.0	\$ Wall Column Line J-a
2053	220.5	274.0	8.0	\$ Wall Column Line J-b
2054	335.0	274.0	8.0	\$ Wall Column Line J-c
2055	388.6	274.0	8.0	\$ Wall Column Line J-d
2056	17.1	180.0	8.0	\$ Wall Column Line L-a
2057	103.5	180.0	8.0	\$ Wall Column Line L-b
2058	1.1	119.0	15.0	\$ Wall Column Line N-a
2059	66.6	119.0	15.0	\$ Wall Column Line N-b
2060	121.9	119.0	15.0	\$ Wall Column Line N-c
2061	378.0	119.0	8.0	\$ Wall Column Line N-d
2062	438.4	119.0	8.0	\$ Wall Column Line N-e
2063	18.4	80.0	8.0	\$ Wall Column Line O-a
2064	77.3	80.0	8.0	\$ Wall Column Line O-b
2065	134.3	80.0	8.0	\$ Wall Column Line O-c
2066	225.9	80.0	8.0	\$ Wall Column Line O-d
2067	305.5	80.0	8.0	\$ Wall Column Line O-e
2068	176.3	50.0	8.0	\$ Wall Column Line P-a
2069	223.8	50.0	8.0	\$ Wall Column Line P-b
2070	274.5	50.0	8.0	\$ Wall Column Line P-c
2071	7.9	0.0	8.0	\$ Wall Column Line R-a
2072	69.1	0.0	8.0	\$ Wall Column Line R-b
2073	134.9	0.0	8.0	\$ Wall Column Line R-c
2074	183.5	0.0	8.0	\$ Wall Column Line R-d
2075	238.5	0.0	8.0	\$ Wall Column Line R-e
2076	305.5	0.0	8.0	\$ Wall Column Line R-f
\$				
\$ Elev. 32				
101	0.0	246.0	32.0	\$ Wall Column Line 1-1
102	48.0	247.3	32.0	\$ Wall Column Line 3-1
103	89.0	281.5	32.0	\$ Wall Column Line 3.5-1
104	123.0	193.8	32.0	\$ Wall Column Line 4-1
105	123.0	295.5	32.0	\$ Wall Column Line 4-2
106	123.0	398.4	32.0	\$ Wall Column Line 4-3
107	147.0	38.9	32.0	\$ Wall Column Line 5-1
108	147.0	122.1	32.0	\$ Wall Column Line 5-2
109	147.0	192.6	32.0	\$ Wall Column Line 5-3
110	147.0	243.5	32.0	\$ Wall Column Line 5-4
111	147.0	295.0	32.0	\$ Wall Column Line 5-5
112	147.0	346.5	32.0	\$ Wall Column Line 5-6
113	147.0	442.5	32.0	\$ Wall Column Line 5-7
114	171.0	80.6	32.0	\$ Wall Column Line 6-1
115	195.0	139.6	32.0	\$ Wall Column Line 7-1
116	195.0	237.0	32.0	\$ Wall Column Line 7-2
117	195.0	412.0	32.0	\$ Wall Column Line 7-3
118	207.0	453.9	32.0	\$ Wall Column Line 7.5-1
119	225.0	388.0	32.0	\$ Wall Column Line 8.3-1
120	259.0	216.5	32.0	\$ Wall Column Line 9-1
121	259.0	386.0	32.0	\$ Wall Column Line 9-2
122	295.0	122.1	32.0	\$ Wall Column Line 10-1
123	295.0	289.0	32.0	\$ Wall Column Line 10-2
124	295.0	386.0	32.0	\$ Wall Column Line 10-3
125	277.0	93.1	32.0	\$ Wall Column Line 9.5-1
126	344.0	133.5	32.0	\$ Wall Column Line 11-1
127	344.0	211.0	32.0	\$ Wall Column Line 11-2
128	344.0	289.0	32.0	\$ Wall Column Line 11-3
129	344.0	373.0	32.0	\$ Wall Column Line 11-4
130	344.0	446.9	32.0	\$ Wall Column Line 11-5
131	377.0	216.8	32.0	\$ Wall Column Line 12-1
132	377.0	289.0	32.0	\$ Wall Column Line 12-2
133	377.0	373.0	32.0	\$ Wall Column Line 12-3
134	442.0	78.1	32.0	\$ Wall Column Line 13-1
135	442.0	210.8	32.0	\$ Wall Column Line 13-2
136	442.0	288.8	32.0	\$ Wall Column Line 13-3
137	442.0	425.9	32.0	\$ Wall Column Line 13-4
\$				
138	221.0	492.0	32.0	\$ Wall Column Line A-1
139	171.0	466.0	32.0	\$ Wall Column Line B-1
140	184.0	414.0	32.0	\$ Wall Column Line D-1
141	95.0	402.0	32.0	\$ Wall Column Line D.5-1
142	119.9	388.0	32.0	\$ Wall Column Line E-1
143	369.1	388.0	32.0	\$ Wall Column Line E-2
144	114.3	362.0	32.0	\$ Wall Column Line F-1
145	246.6	362.0	32.0	\$ Wall Column Line F-2
146	114.3	336.0	32.0	\$ Wall Column Line G-1

147	269.5	336.0	32.0	\$ Wall Column Line G-2
148	210.0	274.0	32.0	\$ Wall Column Line J-5
149	119.9	310.0	32.0	\$ Wall Column Line H-1
150	270.6	310.0	32.0	\$ Wall Column Line H-2
151	119.9	283.5	32.0	\$ Wall Column Line H.75-1
152	305.5	274.0	32.0	\$ Wall Column Line J-1
153	388.9	274.0	32.0	\$ Wall Column Line J-2
154	114.3	257.5	32.0	\$ Wall Column Line J.4-1
155	114.3	231.0	32.0	\$ Wall Column Line J.9-1
156	305.5	226.0	32.0	\$ Wall Column Line K-1
157	339.0	226.0	32.0	\$ Wall Column Line K-2
158	409.5	226.0	32.0	\$ Wall Column Line K-3
159	119.9	204.5	32.0	\$ Wall Column Line K.5-1
160	279.2	204.5	32.0	\$ Wall Column Line K.5-2
161	271.0	192.0	32.0	\$ Wall Column Line K.8-1
162	72.6	180.0	32.0	\$ Wall Column Line L-1
163	396.6	180.0	32.0	\$ Wall Column Line L-2
165	205.0	154.0	32.0	\$ Wall Column Line M-1
166	305.5	154.0	32.0	\$ Wall Column Line M-2
168	56.9	119.0	32.0	\$ Wall Column Line N-1
169	225.5	119.0	32.0	\$ Wall Column Line N-2
170	305.5	119.0	32.0	\$ Wall Column Line N-3
171	388.9	119.0	32.0	\$ Wall Column Line N-4
172	73.6	80.0	32.0	\$ Wall Column Line O-1
173	242.4	80.0	32.0	\$ Wall Column Line O-2
174	388.9	80.0	32.0	\$ Wall Column Line O-3
175	227.1	50.0	32.0	\$ Wall Column Line P-1
176	73.6	0.0	32.0	\$ Wall Column Line R-1
177	242.5	0.0	32.0	\$ Wall Column Line R-2
178	388.9	0.0	32.0	\$ Wall Column Line R-3
179	135.0	136.5	32.0	\$ Wall Column Line 4.5-1
180	147.0	397.8	32.0	\$ Wall Column Line 5-9
181	225.0	290.0	32.0	\$ Wall Column Line 8.3-4
182	410.6	336.0	32.0	\$ Wall Column Line G-3
183	344.0	86.8	32.0	\$ Wall Column Line 11-8
184	384.0	85.3	32.0	\$ Wall Column Line 12.1-1
185	384.0	113.8	32.0	\$ Wall Column Line 12.1-2
186	-17.8	145.0	32.0	\$ Wall Column Line M.3-1
187	69.9	145.0	32.0	\$ Wall Column Line M.3-2
\$				
201	0.0	246.0	32.0	\$ Wall Column Line 1-2
202	48.0	98.1	32.0	\$ Wall Column Line 3-2
203	48.0	297.1	32.0	\$ Wall Column Line 3-3
204	89.0	303.3	32.0	\$ Wall Column Line 3.5-2
205	123.0	296.9	32.0	\$ Wall Column Line 4-4
206	147.0	266.5	32.0	\$ Wall Column Line 5-8
207	171.0	99.5	32.0	\$ Wall Column Line 6-2
208	195.0	310.0	32.0	\$ Wall Column Line 7-4
209	259.0	266.5	32.0	\$ Wall Column Line 9-3
210	295.0	39.9	32.0	\$ Wall Column Line 10-4
211	295.0	266.5	32.0	\$ Wall Column Line 10-5
212	344.0	255.0	32.0	\$ Wall Column Line 11-6
213	442.0	245.4	32.0	\$ Wall Column Line 13-5
\$				
214	221.1	492.0	32.0	\$ Wall Column Line A-2
215	171.0	466.0	32.0	\$ Wall Column Line B-2
216	208.0	414.0	32.0	\$ Wall Column Line D-7
217	99.3	414.0	32.0	\$ Wall Column Line D-2
218	276.5	414.0	32.0	\$ Wall Column Line D-3
219	106.0	402.0	32.0	\$ Wall Column Line D.5-2
220	371.9	388.0	32.0	\$ Wall Column Line E-3
221	210.0	274.0	32.0	\$ Wall Column Line J-6
222	207.0	310.0	32.0	\$ Wall Column Line H-3
223	322.7	310.0	32.0	\$ Wall Column Line H-4
224	396.3	274.0	32.0	\$ Wall Column Line J-3
225	395.9	226.0	32.0	\$ Wall Column Line K-4
226	85.8	192.0	32.0	\$ Wall Column Line K.8-2
227	73.4	180.0	32.0	\$ Wall Column Line L-3
228	395.9	180.0	32.0	\$ Wall Column Line L-4
229	171.0	154.0	32.0	\$ Wall Column Line M-3
230	73.4	119.0	32.0	\$ Wall Column Line N-5
231	301.4	119.0	32.0	\$ Wall Column Line N-6
232	13.6	80.0	32.0	\$ Wall Column Line O-4
233	248.4	80.0	32.0	\$ Wall Column Line O-5
234	222.2	0.0	32.0	\$ Wall Column Line R-4
235	225.0	344.0	32.0	\$ Wall Column Line 8.3-2
236	147.0	442.5	32.0	\$ Wall Column Line 5-10
237	395.6	336.0	32.0	\$ Wall Column Line G-4
238	384.0	99.5	32.0	\$ Wall Column Line 12.1-3
\$ Elev 66				
301	0.0	246.0	66.0	\$ Wall Column Line 1-2
302	48.0	98.1	66.0	\$ Wall Column Line 3-2
303	48.0	297.1	66.0	\$ Wall Column Line 3-3
304	89.0	303.3	66.0	\$ Wall Column Line 3.5-2
305	123.0	296.9	66.0	\$ Wall Column Line 4-4
306	147.0	266.5	66.0	\$ Wall Column Line 5-8

307	171.0	99.5	66.0	\$ Wall Column Line 6-2
308	195.0	310.0	66.0	\$ Wall Column Line 7-4
309	259.0	266.5	66.0	\$ Wall Column Line 9-3
310	295.0	39.9	66.0	\$ Wall Column Line 10-4
311	295.0	266.5	66.0	\$ Wall Column Line 10-5
312	344.0	255.0	66.0	\$ Wall Column Line 11-6
313	442.0	245.4	66.0	\$ Wall Column Line 13-5
\$				
314	221.1	492.0	66.0	\$ Wall Column Line A-2
315	171.0	466.0	66.0	\$ Wall Column Line B-2
316	208.0	414.0	66.0	\$ Wall Column Line D-7
317	99.3	414.0	66.0	\$ Wall Column Line D-2
318	276.5	414.0	66.0	\$ Wall Column Line D-3
319	106.0	402.0	66.0	\$ Wall Column Line D.5-2
320	371.9	388.0	66.0	\$ Wall Column Line E-3
321	210.0	274.0	66.0	\$ Wall Column Line J-6
322	207.0	310.0	66.0	\$ Wall Column Line H-3
323	322.7	310.0	66.0	\$ Wall Column Line H-4
324	396.3	274.0	66.0	\$ Wall Column Line J-3
325	395.9	226.0	66.0	\$ Wall Column Line K-4
326	85.8	192.0	66.0	\$ Wall Column Line K.8-2
327	73.4	180.0	66.0	\$ Wall Column Line L-3
328	395.9	180.0	66.0	\$ Wall Column Line L-4
329	171.0	154.0	66.0	\$ Wall Column Line M-3
330	73.4	119.0	66.0	\$ Wall Column Line N-5
331	301.4	119.0	66.0	\$ Wall Column Line N-6
332	13.6	80.0	66.0	\$ Wall Column Line O-4
333	248.4	80.0	66.0	\$ Wall Column Line O-5
334	222.2	0.0	66.0	\$ Wall Column Line R-4
335	225.0	344.0	66.0	\$ Wall Column Line 8.3-2
336	147.0	442.5	66.0	\$ Wall Column Line 5-10
337	395.6	336.0	66.0	\$ Wall Column Line G-4
338	384.0	99.5	66.0	\$ Wall Column Line 12.1-3
\$				
401	0.0	235.3	66.0	\$ Wall Column Line 1-3
402	48.0	299.5	66.0	\$ Wall Column Line 3-4
403	123.0	296.8	66.0	\$ Wall Column Line 4-5
404	195.0	344.0	66.0	\$ Wall Column Line 7-5
405	225.0	344.0	66.0	\$ Wall Column Line 8.3-3
406	259.0	266.5	66.0	\$ Wall Column Line 9-4
407	295.0	39.9	66.0	\$ Wall Column Line 10-6
408	295.0	266.5	66.0	\$ Wall Column Line 10-7
409	344.0	252.5	66.0	\$ Wall Column Line 11-7
\$				
410	221.1	492.0	66.0	\$ Wall Column Line A-3
411	210.0	414.0	66.0	\$ Wall Column Line D-8
412	83.8	414.0	66.0	\$ Wall Column Line D-4
413	276.5	414.0	66.0	\$ Wall Column Line D-5
414	368.4	388.0	66.0	\$ Wall Column Line E-4
415	210.0	274.0	66.0	\$ Wall Column Line J-7
416	207.0	310.0	66.0	\$ Wall Column Line H-5
417	319.3	310.0	66.0	\$ Wall Column Line H-6
418	394.4	274.0	66.0	\$ Wall Column Line J-4
419	393.6	226.0	66.0	\$ Wall Column Line K-5
420	88.5	180.0	66.0	\$ Wall Column Line L-5
421	393.6	180.0	66.0	\$ Wall Column Line L-6
422	142.9	119.0	66.0	\$ Wall Column Line N-7
423	305.6	119.0	66.0	\$ Wall Column Line N-8
424	282.6	80.0	66.0	\$ Wall Column Line O-6
425	223.3	0.0	66.0	\$ Wall Column Line R-5
426	442.0	245.5	66.0	\$ Wall Column Line 13-6
427	393.1	336.0	66.0	\$ Wall Column Line G-5
428	123.0	99.5	66.0	\$ Wall Column Line 4-7
429	384.0	99.5	66.0	\$ Wall Column Line 12.1-4
\$ Elev 100				
501	0.0	235.3	100.0	\$ Wall Column Line 1-3
502	48.0	299.5	100.0	\$ Wall Column Line 3-4
503	123.0	296.8	100.0	\$ Wall Column Line 4-5
504	195.0	344.0	100.0	\$ Wall Column Line 7-5
505	225.0	344.0	100.0	\$ Wall Column Line 8.3-3
506	259.0	266.5	100.0	\$ Wall Column Line 9-4
507	295.0	39.9	100.0	\$ Wall Column Line 10-6
508	295.0	266.5	100.0	\$ Wall Column Line 10-7
509	344.0	252.5	100.0	\$ Wall Column Line 11-7
\$				
510	221.1	492.0	100.0	\$ Wall Column Line A-3
511	210.0	414.0	100.0	\$ Wall Column Line D-8
512	83.8	414.0	100.0	\$ Wall Column Line D-4
513	276.5	414.0	100.0	\$ Wall Column Line D-5
514	368.4	388.0	100.0	\$ Wall Column Line E-4
515	210.0	274.0	100.0	\$ Wall Column Line J-7
516	207.0	310.0	100.0	\$ Wall Column Line H-5
517	319.3	310.0	100.0	\$ Wall Column Line H-6
518	394.4	274.0	100.0	\$ Wall Column Line J-4
519	393.6	226.0	100.0	\$ Wall Column Line K-5
520	88.5	180.0	100.0	\$ Wall Column Line L-5

521	393.6	180.0	100.0	\$ Wall Column Line L-6
522	142.9	119.0	100.0	\$ Wall Column Line N-7
523	305.6	119.0	100.0	\$ Wall Column Line N-8
524	282.6	80.0	100.0	\$ Wall Column Line O-6
525	223.3	0.0	100.0	\$ Wall Column Line R-5
526	442.0	245.5	100.0	\$ Wall Column Line 13-6
527	393.1	336.0	100.0	\$ Wall Column Line G-5
528	123.0	99.5	100.0	\$ Wall Column Line 4-7
529	384.0	99.5	100.0	\$ Wall Column Line 12.1-4
\$				
601	48.0	297.3	100.0	\$ Wall Column Line 3-5
602	123.0	296.8	100.0	\$ Wall Column Line 4-6
\$				
603	85.0	414.0	100.0	\$ Wall Column Line D-6
604	91.5	180.0	100.0	\$ Wall Column Line L-7
\$ Elev 107				
701	48.0	297.3	107.0	\$ Wall Column Line 3-5
702	123.0	296.8	107.0	\$ Wall Column Line 4-6
\$				
703	85.0	414.0	107.0	\$ Wall Column Line D-6
704	91.5	180.0	107.0	\$ Wall Column Line L-7
\$ Master Nodes (Center of Rigidity) and Center of Mass Nodes				
99	212.45	253.53	-4.0	\$ Center of Mass at EL. 0.0
100	221.00	246.00	-4.0	\$ Master Node at Base slab (Center of Rigidity)
199	211.17	247.27	31.5	\$ Center of Mass at EL. 31.5
200	204.81	244.91	31.5	\$ Master Node at EL. 31.5 (Center of Rigidity)
399	207.22	247.93	65.5	\$ Center of Mass at EL. 65.5
400	206.53	223.49	65.5	\$ Master Node at EL. 65.5 (Center of Rigidity)
599	243.24	237.19	99.5	\$ Center of Mass at EL. 99.5
600	230.62	222.66	99.5	\$ Master Node at EL. 99.5 (Center of Rigidity)
700	85.50	297.00	106.5	\$ Master Node at EL. 106.5 (Center of Rigidity and Center of Mass)
\$				
TYPE SPACE FRAME				
MEMBER INCIDENCES				
'1-1'	1	101		
'1-a'	1000	2000		
'1-b'	1001	2001		
'1-c'	1002	2002		
'1-d'	1003	2003		
'1-e'	1004	2004		
'1-f'	1005	2005		
'1-2'	201	301		
'1-3'	401	501		
'3-1'	2	102		
'3-a'	1006	2006		
'3-b'	1007	2007		
'3-c'	1008	2008		
'3-d'	1009	2009		
'3-e'	1010	2010		
'3-2'	202	302		
'3-3'	203	303		
'3-4'	402	502		
'3-5'	601	701		
'3.5-1'	3	103		
'3.5-2'	204	304		
'3.5-a'	1011	2011		
'3.5-b'	1012	2012		
'3.5-c'	1013	2013		
'3.5-d'	1014	2014		
'3.5-e'	1015	2015		
'4-1'	4	104		
'4-a'	1016	2016		
'4-b'	1017	2017		
'4-2'	5	105		
'4-3'	6	106		
'4-4'	205	305		
'4-5'	403	503		
'4-6'	602	702		
'4-7'	428	528		
'4.5-1'	79	179		
'5-1'	7	107		
'5-2'	8	108		
'5-3'	9	109		
'5-4'	10	110		
'5-5'	11	111		
'5-6'	12	112		
'5-7'	13	113		
'5-a'	1018	2018		
'5-b'	1019	2019		
'5-8'	206	306		
'5-9'	80	180		
'5-10'	236	336		
'6-1'	14	114		
'6-2'	207	307		
'7-1'	15	115		
'7-2'	16	116		

'7-3'	17	117
'7-4'	208	308
'7-5'	404	504
'7.5-1'	18	118
'8.3-1'	19	119
'8.3-2'	235	335
'8.3-3'	405	505
'8.3-4'	81	181
'8.3-a'	1020	2020
'8.3-b'	1021	2021
'9-1'	20	120
'9-2'	21	121
'9-3'	209	309
'9-4'	406	506
'9-a'	1022	2022
'9-b'	1023	2023
'9-c'	1024	2024
'10-1'	22	122
'10-2'	23	123
'10-3'	24	124
'10-4'	210	310
'10-5'	211	311
'10-6'	407	507
'10-7'	408	508
'10-a'	1025	2025
'10-b'	1026	2026
'10-c'	1027	2027
'10-d'	1028	2028
'10-e'	1029	2029
'10-f'	1030	2030
'10-g'	1031	2031
'9.5-1'	25	125
'11-1'	26	126
'11-2'	27	127
'11-3'	28	128
'11-4'	29	129
'11-5'	30	130
'11-6'	212	312
'11-7'	409	509
'11-8'	83	183
'11-a'	1032	2032
'11-b'	1033	2033
'11-c'	1034	2034
'11-d'	1035	2035
'12-1'	31	131
'12-2'	32	132
'12-3'	33	133
'12-a'	1036	2036
'12-b'	1037	2037
'12.1-1'	84	184
'12.1-2'	85	185
'12.1-3'	238	338
'12.1-4'	429	529
'13-1'	34	134
'13-2'	35	135
'13-3'	36	136
'13-4'	37	137
'13-5'	213	313
'13-6'	426	526
'13-a'	1038	2038
'13-b'	1039	2039
'13-c'	1040	2040
'13-d'	1041	2041
'13-e'	1042	2042
'13-f'	1043	2043
'A-1'	38	138
'A-a'	1044	2044
'A-b'	1045	2045
'A-c'	1046	2046
'A-2'	214	314
'A-3'	410	510
'B-1'	39	139
'B-2'	215	315
'D-1'	40	140
'D-a'	1047	2047
'D-b'	1048	2048
'D-c'	1049	2049
'D-2'	217	317
'D-3'	218	318
'D-4'	412	512
'D-5'	413	513
'D-6'	603	703
'D-7'	216	316
'D-8'	411	511
'D.5-1'	41	141
'D.5-2'	219	319

'E-1'	42	142
'E-2'	43	143
'E-a'	1050	2050
'E-b'	1051	2051
'E-3'	220	320
'E-4'	414	514
'F-1'	44	144
'F-2'	45	145
'G-1'	46	146
'G-2'	47	147
'G-3'	82	182
'G-4'	237	337
'G-5'	427	527
'H-1'	49	149
'H-2'	50	150
'H-3'	222	322
'H-4'	223	323
'H-5'	416	516
'H-6'	417	517
'H.75-1'	51	151
'J-1'	52	152
'J-2'	53	153
'J-c'	1054	2054
'J-d'	1055	2055
'J-3'	224	324
'J-4'	418	518
'J-5'	48	148
'J-a'	1052	2052
'J-b'	1053	2053
'J-6'	221	321
'J-7'	415	515
'J.4-1'	54	154
'J.9-1'	55	155
'K-1'	56	156
'K-2'	57	157
'K-3'	58	158
'K-4'	225	325
'K-5'	419	519
'K.5-1'	59	159
'K.5-2'	60	160
'K.8-1'	61	161
'K.8-2'	226	326
'L-1'	62	162
'L-a'	1056	2056
'L-b'	1057	2057
'L-2'	63	163
'L-3'	227	327
'L-4'	228	328
'L-5'	420	520
'L-6'	421	521
'L-7'	604	704
'M-1'	65	165
'M-2'	66	166
'M-3'	229	329
'M.3-1'	86	186
'M.3-2'	87	187
'N-1'	68	168
'N-a'	1058	2058
'N-b'	1059	2059
'N-c'	1060	2060
'N-2'	69	169
'N-3'	70	170
'N-4'	71	171
'N-d'	1061	2061
'N-e'	1062	2062
'N-5'	230	330
'N-6'	231	331
'N-7'	422	522
'N-8'	423	523
'O-1'	72	172
'O-a'	1063	2063
'O-b'	1064	2064
'O-c'	1065	2065
'O-2'	73	173
'O-d'	1066	2066
'O-e'	1067	2067
'O-3'	74	174
'O-4'	232	332
'O-5'	233	333
'O-6'	424	524
'P-1'	75	175
'P-a'	1068	2068
'P-b'	1069	2069
'P-c'	1070	2070
'R-1'	76	176
'R-a'	1071	2071

'R-b'	1072	2072
'R-c'	1073	2073
'R-2'	77	177
'R-d'	1074	2074
'R-e'	1075	2075
'R-f'	1076	2076
'R-3'	78	178
'R-4'	234	334
'R-5'	425	525

\$		
'dummy 1'	199	200
'dummy 2'	399	400
'dummy 3'	599	600
'dummy 4'	99	100

\$  
CONSTANTS

E	617302.00	MEMBERS	ALL
POISSON	0.17	MEMBERS	ALL
G	263804.27	MEMBERS	ALL
DENSITY	0.000000001	MEMBERS	ALL

\$			
BETA	90.000000000	MEMBER	'A-1'
BETA	90.000000000	MEMBER	'A-a'
BETA	90.000000000	MEMBER	'A-b'
BETA	90.000000000	MEMBER	'A-c'
BETA	90.000000000	MEMBER	'A-2'
BETA	90.000000000	MEMBER	'A-3'
BETA	90.000000000	MEMBER	'B-1'
BETA	90.000000000	MEMBER	'B-2'
BETA	90.000000000	MEMBER	'D-1'
BETA	90.000000000	MEMBER	'D-a'
BETA	90.000000000	MEMBER	'D-b'
BETA	90.000000000	MEMBER	'D-c'
BETA	90.000000000	MEMBER	'D-2'
BETA	90.000000000	MEMBER	'D-3'
BETA	90.000000000	MEMBER	'D-4'
BETA	90.000000000	MEMBER	'D-5'
BETA	90.000000000	MEMBER	'D-6'
BETA	90.000000000	MEMBER	'D-7'
BETA	90.000000000	MEMBER	'D-8'
BETA	90.000000000	MEMBER	'D.5-1'
BETA	90.000000000	MEMBER	'D.5-2'
BETA	90.000000000	MEMBER	'E-1'
BETA	90.000000000	MEMBER	'E-2'
BETA	90.000000000	MEMBER	'E-a'
BETA	90.000000000	MEMBER	'E-b'
BETA	90.000000000	MEMBER	'E-3'
BETA	90.000000000	MEMBER	'E-4'
BETA	90.000000000	MEMBER	'F-1'
BETA	90.000000000	MEMBER	'F-2'
BETA	90.000000000	MEMBER	'G-1'
BETA	90.000000000	MEMBER	'G-2'
BETA	90.000000000	MEMBER	'G-3'
BETA	90.000000000	MEMBER	'G-4'
BETA	90.000000000	MEMBER	'G-5'
BETA	90.000000000	MEMBER	'H-1'
BETA	90.000000000	MEMBER	'H-2'
BETA	90.000000000	MEMBER	'H-3'
BETA	90.000000000	MEMBER	'H-4'
BETA	90.000000000	MEMBER	'H-5'
BETA	90.000000000	MEMBER	'H-6'
BETA	90.000000000	MEMBER	'H.75-1'
BETA	90.000000000	MEMBER	'J-1'
BETA	90.000000000	MEMBER	'J-2'
BETA	90.000000000	MEMBER	'J-c'
BETA	90.000000000	MEMBER	'J-d'
BETA	90.000000000	MEMBER	'J-3'
BETA	90.000000000	MEMBER	'J-4'
BETA	90.000000000	MEMBER	'J-5'
BETA	90.000000000	MEMBER	'J-a'
BETA	90.000000000	MEMBER	'J-b'
BETA	90.000000000	MEMBER	'J-6'
BETA	90.000000000	MEMBER	'J-7'
BETA	90.000000000	MEMBER	'J.4-1'
BETA	90.000000000	MEMBER	'J.9-1'
BETA	90.000000000	MEMBER	'K-1'
BETA	90.000000000	MEMBER	'K-2'
BETA	90.000000000	MEMBER	'K-3'
BETA	90.000000000	MEMBER	'K-4'
BETA	90.000000000	MEMBER	'K-5'
BETA	90.000000000	MEMBER	'K.5-1'
BETA	90.000000000	MEMBER	'K.5-2'
BETA	90.000000000	MEMBER	'K.8-1'
BETA	90.000000000	MEMBER	'K.8-2'
BETA	90.000000000	MEMBER	'L-1'
BETA	90.000000000	MEMBER	'L-a'

BETA 90.000000000 MEMBER 'L-b'  
BETA 90.000000000 MEMBER 'L-2'  
BETA 90.000000000 MEMBER 'L-3'  
BETA 90.000000000 MEMBER 'L-4'  
BETA 90.000000000 MEMBER 'L-5'  
BETA 90.000000000 MEMBER 'L-6'  
BETA 90.000000000 MEMBER 'L-7'  
BETA 90.000000000 MEMBER 'M-1'  
BETA 90.000000000 MEMBER 'M-2'  
BETA 90.000000000 MEMBER 'M-3'  
BETA 90.000000000 MEMBER 'M.3-1'  
BETA 90.000000000 MEMBER 'M.3-2'  
BETA 90.000000000 MEMBER 'N-1'  
BETA 90.000000000 MEMBER 'N-a'  
BETA 90.000000000 MEMBER 'N-b'  
BETA 90.000000000 MEMBER 'N-c'  
BETA 90.000000000 MEMBER 'N-2'  
BETA 90.000000000 MEMBER 'N-3'  
BETA 90.000000000 MEMBER 'N-4'  
BETA 90.000000000 MEMBER 'N-d'  
BETA 90.000000000 MEMBER 'N-e'  
BETA 90.000000000 MEMBER 'N-5'  
BETA 90.000000000 MEMBER 'N-6'  
BETA 90.000000000 MEMBER 'N-7'  
BETA 90.000000000 MEMBER 'N-8'  
BETA 90.000000000 MEMBER 'O-1'  
BETA 90.000000000 MEMBER 'O-a'  
BETA 90.000000000 MEMBER 'O-b'  
BETA 90.000000000 MEMBER 'O-c'  
BETA 90.000000000 MEMBER 'O-2'  
BETA 90.000000000 MEMBER 'O-d'  
BETA 90.000000000 MEMBER 'O-e'  
BETA 90.000000000 MEMBER 'O-3'  
BETA 90.000000000 MEMBER 'O-4'  
BETA 90.000000000 MEMBER 'O-5'  
BETA 90.000000000 MEMBER 'O-6'  
BETA 90.000000000 MEMBER 'P-1'  
BETA 90.000000000 MEMBER 'P-a'  
BETA 90.000000000 MEMBER 'P-b'  
BETA 90.000000000 MEMBER 'P-c'  
BETA 90.000000000 MEMBER 'R-1'  
BETA 90.000000000 MEMBER 'R-a'  
BETA 90.000000000 MEMBER 'R-b'  
BETA 90.000000000 MEMBER 'R-c'  
BETA 90.000000000 MEMBER 'R-2'  
BETA 90.000000000 MEMBER 'R-d'  
BETA 90.000000000 MEMBER 'R-e'  
BETA 90.000000000 MEMBER 'R-f'  
BETA 90.000000000 MEMBER 'R-3'  
BETA 90.000000000 MEMBER 'R-4'  
BETA 90.000000000 MEMBER 'R-5'

\$

MEMBER PROPERTIES PRISMATIC

'1-1'	AX	2997.0	AY	2497.5	AZ	0.001	IX	35964.0	IY	8991.0	IZ	62312687.4
'1-a'	AX	427.5	AY	356.3	AZ	0.001	IX	5130.0	IY	1282.5	IZ	180852.5
'1-b'	AX	312.0	AY	260.0	AZ	0.001	IX	3744.0	IY	936.0	IZ	70304.0
'1-c'	AX	253.5	AY	211.3	AZ	0.001	IX	3042.0	IY	760.5	IZ	37709.4
'1-d'	AX	388.5	AY	323.8	AZ	0.001	IX	4662.0	IY	1165.5	IZ	135734.2
'1-e'	AX	834.0	AY	695.0	AZ	0.001	IX	10008.0	IY	2502.0	IZ	1342809.5
'1-f'	AX	496.5	AY	413.8	AZ	0.001	IX	5958.0	IY	1489.5	IZ	283317.9
\$												
'1-2'	AX	2234.3	AY	1820.3	AZ	0.001	-					
	IX	13995.3	IY	3498.8	IZ	45897499.5						
'1-3'	AX	1489.5	AY	1138.4	AZ	0.001	-					
	IX	4153.5	IY	1038.4	IZ	30598333.0						
\$												
'3-1'	AX	1350.0	AY	1125.0	AZ	0.001	IX	7200.0	IY	1800.0	IZ	12814453.1
'3-a'	AX	99.0	AY	82.5	AZ	0.001	IX	528.0	IY	132.0	IZ	5053.6
'3-b'	AX	57.0	AY	47.5	AZ	0.001	IX	304.0	IY	76.0	IZ	964.5
'3-c'	AX	169.0	AY	140.8	AZ	0.001	IX	901.3	IY	225.3	IZ	25139.6
'3-d'	AX	285.0	AY	237.5	AZ	0.001	IX	1520.0	IY	380.0	IZ	120568.4
'3-e'	AX	538.0	AY	448.3	AZ	0.001	IX	2869.3	IY	717.3	IZ	811046.2
\$												
'3-2'	AX	107.5	AY	89.6	AZ	0.001	-					
	IX	580.7	IY	145.2	IZ	301695.0						
'3-3'	AX	726.8	AY	589.6	AZ	0.001	-					
	IX	1995.8	IY	498.9	IZ	3554114.1						
'3-4'	AX	712.5	AY	582.6	AZ	0.001	-					
	IX	2007.0	IY	501.8	IZ	3349121.1						
'3-5'	AX	712.5	AY	593.8	AZ	0.001	-					
	IX	2137.5	IY	534.4	IZ	3349121.1						
\$												
'3.5-1'	AX	1076.0	AY	896.7	AZ	0.001	IX	5738.7	IY	1434.7	IZ	6488369.7
'3.5-a'	AX	140.0	AY	116.7	AZ	0.001	IX	746.7	IY	186.7	IZ	14291.7
'3.5-b'	AX	197.0	AY	164.2	AZ	0.001	IX	1050.7	IY	262.7	IZ	39819.7



'3.5-c'	AX	177.0	AY	147.5	AZ	0.001	IX	944.0	IY	236.0	IZ	28881.4
'3.5-d'	AX	178.0	AY	148.3	AZ	0.001	IX	949.3	IY	237.3	IZ	29373.7
'3.5-e'	AX	208.0	AY	173.3	AZ	0.001	IX	1109.3	IY	277.3	IZ	46869.3
\$												
'3.5-2'	AX	904.0	AY	734.7	AZ	0.001	-					
	IX	4352.0	IY	1088.0	IZ	3847725.3						
'4-1'	AX	114.0	AY	87.8	AZ	0.001	-					
	IX	458.7	IY	114.7	IZ	3312.8						
\$												
'4-2'	AX	112.0	AY	93.3	AZ	0.001	IX	597.3	IY	149.3	IZ	7317.3
'4-a'	AX	36.0	AY	30.0	AZ	0.001	IX	192.0	IY	48.0	IZ	243.0
'4-b'	AX	36.0	AY	30.0	AZ	0.001	IX	192.0	IY	48.0	IZ	243.0
\$												
'4-3'	AX	126.0	AY	95.5	AZ	0.001	-					
	IX	480.0	IY	120.0	IZ	3796.9						
'4-4'	AX	952.0	AY	787.5	AZ	0.001	-					
	IX	4922.7	IY	1230.7	IZ	3465468.8						
'4-5'	AX	712.5	AY	593.8	AZ	0.001	-					
	IX	2137.5	IY	534.4	IZ	3349121.1						
'4-6'	AX	712.5	AY	593.8	AZ	0.001	-					
	IX	2137.5	IY	534.4	IZ	3349121.1						
'4-7'	AX	172.0	AY	143.3	AZ	0.001	-					
	IX	917.3	IY	229.3	IZ	26502.3						
'4.5-1'	AX	156.0	AY	130.0	AZ	0.001	-					
	IX	832.0	IY	208.0	IZ	19773.0						
'5-1'	AX	341.0	AY	284.2	AZ	0.001	-					
	IX	1818.7	IY	454.7	IZ	206519.9						
'5-2'	AX	305.0	AY	254.2	AZ	0.001	-					
	IX	1626.7	IY	406.7	IZ	147774.1						
'5-3'	AX	143.0	AY	119.2	AZ	0.001	-					
	IX	762.7	IY	190.7	IZ	15230.2						
'5-4'	AX	156.0	AY	130.0	AZ	0.001	-					
	IX	832.0	IY	208.0	IZ	19773.0						
'5-5'	AX	144.0	AY	120.0	AZ	0.001	-					
	IX	768.0	IY	192.0	IZ	15552.0						
'5-6'	AX	156.0	AY	130.0	AZ	0.001	-					
	IX	832.0	IY	208.0	IZ	19773.0						
\$												
'5-7'	AX	200.0	AY	166.7	AZ	0.001	IX	1066.7	IY	266.7	IZ	41666.7
'5-a'	AX	64.0	AY	53.3	AZ	0.001	IX	341.3	IY	85.3	IZ	1365.3
'5-b'	AX	108.0	AY	90.0	AZ	0.001	IX	576.0	IY	144.0	IZ	6561.0
\$												
'5-8'	AX	1196.0	AY	996.7	AZ	0.001	-					
	IX	6378.7	IY	1594.7	IZ	8910299.7						
'5-9'	AX	142.0	AY	118.3	AZ	0.001	-					
	IX	757.3	IY	189.3	IZ	14913.0						
'5-10'	AX	200.0	AY	166.7	AZ	0.001	-					
	IX	1066.7	IY	266.7	IZ	41666.7						
'6-1'	AX	603.0	AY	502.5	AZ	0.001	-					
	IX	3216.0	IY	804.0	IZ	1141959.5						
'6-2'	AX	172.0	AY	143.3	AZ	0.001	-					
	IX	917.3	IY	229.3	IZ	26502.3						
'7-1'	AX	131.0	AY	109.2	AZ	0.001	-					
	IX	698.7	IY	174.7	IZ	11708.8						
'7-2'	AX	632.0	AY	526.7	AZ	0.001	-					
	IX	3370.7	IY	842.7	IZ	1314770.7						
'7-3'	AX	448.0	AY	373.3	AZ	0.001	-					
	IX	2389.3	IY	597.3	IZ	468309.3						
'7-4'	AX	1264.0	AY	1053.3	AZ	0.001	-					
	IX	6741.3	IY	1685.3	IZ	10518165.3						
'7-5'	AX	576.0	AY	480.0	AZ	0.001	-					
	IX	3072.0	IY	768.0	IZ	995328.0						
'7.5-1'	AX	251.3	AY	209.4	AZ	0.001	-					
	IX	753.8	IY	188.4	IZ	146856.9						
\$												
'8.3-1'	AX	224.0	AY	186.7	AZ	0.001	IX	1194.7	IY	298.7	IZ	58538.7
'8.3-a'	AX	118.0	AY	98.3	AZ	0.001	IX	629.3	IY	157.3	IZ	8557.5
'8.3-b'	AX	44.0	AY	36.7	AZ	0.001	IX	234.7	IY	58.7	IZ	443.7
\$												
'8.3-2'	AX	576.0	AY	480.0	AZ	0.001	-					
	IX	3072.0	IY	768.0	IZ	995328.0						
'8.3-3'	AX	576.0	AY	480.0	AZ	0.001	-					
	IX	3072.0	IY	768.0	IZ	995328.0						
'8.3-4'	AX	124.0	AY	124.3	AZ	0.001	-					
	IX	661.3	IY	165.3	IZ	9930.3						
\$												
'9-1'	AX	796.0	AY	663.3	AZ	0.001	IX	4245.3	IY	1061.3	IZ	2626866.3
'9-a'	AX	292.0	AY	243.3	AZ	0.001	IX	1557.3	IY	389.3	IZ	129672.3
'9-b'	AX	420.0	AY	350.0	AZ	0.001	IX	2240.0	IY	560.0	IZ	385875.0
'9-c'	AX	32.0	AY	26.7	AZ	0.001	IX	170.7	IY	42.7	IZ	170.7
\$												
'9-2'	AX	300.0	AY	250.0	AZ	0.001	-					
	IX	2500.0	IY	625.0	IZ	90000.0						
'9-3'	AX	1196.0	AY	996.7	AZ	0.001	-					
	IX	6378.7	IY	1594.7	IZ	8910299.7						
'9-4'	AX	1196.0	AY	996.7	AZ	0.001	-					

	IX	6378.7	IY	1594.7	IZ	8910299.7						
\$												
'10-1'	AX	1007.0	AY	839.2	AZ	0.001	IX	5370.7	IY	1342.7	IZ	5318475.7
'10-a'	AX	71.0	AY	59.2	AZ	0.001	IX	378.7	IY	94.7	IZ	1864.1
'10-b'	AX	194.0	AY	161.7	AZ	0.001	IX	1034.7	IY	258.7	IZ	38028.0
'10-c'	AX	480.0	AY	400.0	AZ	0.001	IX	2560.0	IY	640.0	IZ	576000.0
'10-d'	AX	200.0	AY	166.7	AZ	0.001	IX	1066.7	IY	266.7	IZ	41666.7
'10-2'	AX	216.0	AY	180.0	AZ	0.001	IX	1152.0	IY	288.0	IZ	52488.0
'10-e'	AX	62.0	AY	51.7	AZ	0.001	IX	330.7	IY	82.7	IZ	1241.3
'10-f'	AX	90.0	AY	75.0	AZ	0.001	IX	480.0	IY	120.0	IZ	3796.9
'10-g'	AX	32.0	AY	26.7	AZ	0.001	IX	170.7	IY	42.7	IZ	170.7
\$												
'10-3'	AX	300.0	AY	250.0	AZ	0.001	-					
	IX	2500.0	IY	625.0	IZ	90000.0						
'10-4'	AX	337.0	AY	280.8	AZ	0.001	-					
	IX	1797.3	IY	449.3	IZ	199337.3						
'10-5'	AX	1196.0	AY	996.7	AZ	0.001	-					
	IX	6378.7	IY	1594.7	IZ	8910299.7						
'10-6'	AX	337.0	AY	280.8	AZ	0.001	-					
	IX	1797.3	IY	449.3	IZ	199337.3						
'10-7'	AX	1196.0	AY	996.7	AZ	0.001	-					
	IX	6378.7	IY	1594.7	IZ	8910299.7						
'9.5-1'	AX	775.0	AY	645.8	AZ	0.001	-					
	IX	4133.3	IY	1033.3	IZ	2424397.8						
'11-1'	AX	159.0	AY	132.5	AZ	0.001	-					
	IX	477.0	IY	119.3	IZ	37219.3						
\$												
'11-2'	AX	222.0	AY	185.0	AZ	0.001	IX	666.0	IY	166.5	IZ	101306.0
'11-a'	AX	22.5	AY	18.8	AZ	0.001	IX	67.5	IY	16.9	IZ	105.5
'11-b'	AX	175.5	AY	146.3	AZ	0.001	IX	526.5	IY	131.6	IZ	50050.4
'11-3'	AX	162.0	AY	135.0	AZ	0.001	IX	486.0	IY	121.5	IZ	39366.0
'11-c'	AX	40.5	AY	33.8	AZ	0.001	IX	121.5	IY	30.4	IZ	615.1
'11-d'	AX	106.5	AY	88.8	AZ	0.001	IX	319.5	IY	79.9	IZ	11184.7
\$												
'11-4'	AX	102.0	AY	85.0	AZ	0.001	-					
	IX	306.0	IY	76.5	IZ	9826.0						
'11-5'	AX	293.3	AY	244.4	AZ	0.001	-					
	IX	879.8	IY	219.9	IZ	233501.8						
'11-6'	AX	813.0	AY	647.2	AZ	0.001	-					
	IX	2034.0	IY	508.5	IZ	4975627.8						
'11-7'	AX	813.0	AY	677.5	AZ	0.001	-					
	IX	2439.0	IY	609.8	IZ	4975627.8						
'11-8'	AX	45.0	AY	28.3	AZ	0.001	-					
	IX	58.5	IY	14.6	IZ	843.8						
'12-1'	AX	208.5	AY	161.2	AZ	0.001	-					
	IX	477.0	IY	119.3	IZ	37219.3						
\$												
'12-2'	AX	162.0	AY	135.0	AZ	0.001	IX	486.0	IY	121.5	IZ	39366.0
'12-a'	AX	18.0	AY	15.0	AZ	0.001	IX	54.0	IY	13.5	IZ	54.0
'12-b'	AX	96.0	AY	80.0	AZ	0.001	IX	288.0	IY	72.0	IZ	8192.0
\$												
'12-3'	AX	102.0	AY	85.0	AZ	0.001	-					
	IX	306.0	IY	76.5	IZ	9826.0						
'12.1-1'	AX	58.0	AY	48.3	AZ	0.001	-					
	IX	309.3	IY	77.3	IZ	1016.2						
'12.1-2'	AX	58.0	AY	48.3	AZ	0.001	-					
	IX	309.3	IY	77.3	IZ	1016.2						
'12.1-3'	AX	172.0	AY	143.3	AZ	0.001	-					
	IX	917.3	IY	229.3	IZ	26502.3						
'12.1-4'	AX	172.0	AY	143.3	AZ	0.001	-					
	IX	917.3	IY	229.3	IZ	26502.3						
\$												
'13-1'	AX	982.5	AY	818.8	AZ	0.001	IX	11790.0	IY	2947.5	IZ	2195401.4
'13-a'	AX	489.0	AY	407.5	AZ	0.001	IX	5868.0	IY	1467.0	IZ	270671.7
'13-b'	AX	441.0	AY	367.5	AZ	0.001	IX	5292.0	IY	1323.0	IZ	198532.7
'13-2'	AX	441.0	AY	367.5	AZ	0.001	IX	5292.0	IY	1323.0	IZ	198532.7
'13-3'	AX	327.0	AY	272.5	AZ	0.001	IX	3924.0	IY	981.0	IZ	80939.3
'13-c'	AX	84.0	AY	70.0	AZ	0.001	IX	1008.0	IY	252.0	IZ	1372.0
'13-d'	AX	192.0	AY	160.0	AZ	0.001	IX	2304.0	IY	576.0	IZ	16384.0
'13-4'	AX	838.5	AY	698.8	AZ	0.001	IX	10062.0	IY	2515.5	IZ	1364663.1
'13-e'	AX	204.0	AY	170.0	AZ	0.001	IX	2448.0	IY	612.0	IZ	19652.0
'13-f'	AX	586.5	AY	488.8	AZ	0.001	IX	7038.0	IY	1759.5	IZ	467003.7
\$												
'13-5'	AX	2234.3	AY	1850.6	AZ	0.001	-					
	IX	14701.5	IY	3675.4	IZ	45897499.5						
'13-6'	AX	1489.5	AY	1229.4	AZ	0.001	-					
	IX	4293.0	IY	1073.3	IZ	30598333.0						
'A-1'	AX	2697.0	AY	2247.5	AZ	0.001	IX	32364.0	IY	8091.0	IZ	45410793.7
'A-a'	AX	685.5	AY	571.3	AZ	0.001	IX	8226.0	IY	2056.5	IZ	745656.2
'A-b'	AX	481.5	AY	401.3	AZ	0.001	IX	5778.0	IY	1444.5	IZ	258407.5
'A-c'	AX	1330.5	AY	1108.8	AZ	0.001	IX	15966.0	IY	3991.5	IZ	5452063.3
'A-2'	AX	2009.3	AY	1669.0	AZ	0.001	-					
	IX	13380.2	IY	3345.0	IZ	33380716.7						
'A-3'	AX	1339.5	AY	1112.7	AZ	0.001	-					
	IX	3964.5	IY	991.1	IZ	22253811.2						
'B-1'	AX	208.0	AY	173.3	AZ	0.001	-					

	IX	1109.3	IY	277.3	IZ	46869.3						
'B-2'	AX	208.0	AY	173.3	AZ	0.001	-					
	IX	1109.3	IY	277.3	IZ	46869.3						
'D-1'	AX	1104.0	AY	920.0	AZ	0.001	IX	5888.0	IY	1472.0	IZ	7008192.0
'D-a'	AX	520.0	AY	433.3	AZ	0.001	IX	2773.3	IY	693.3	IZ	732333.3
'D-b'	AX	124.0	AY	103.3	AZ	0.001	IX	661.3	IY	165.3	IZ	9930.3
'D-c'	AX	272.0	AY	226.7	AZ	0.001	IX	1450.7	IY	362.7	IZ	104810.7
'D-2'	AX	426.0	AY	352.2	AZ	0.001	-					
	IX	2197.3	IY	549.3	IZ	402649.9						
'D-3'	AX	160.0	AY	133.3	AZ	0.001	-					
	IX	853.3	IY	213.3	IZ	21333.3						
'D-4'	AX	234.0	AY	191.3	AZ	0.001	-					
	IX	648.0	IY	162.0	IZ	118638.0						
'D-5'	AX	160.0	AY	133.3	AZ	0.001	-					
	IX	853.3	IY	213.3	IZ	21333.3						
'D-6'	AX	234.0	AY	195.0	AZ	0.001	-					
	IX	702.0	IY	175.5	IZ	118638.0						
'D-7'	AX	148.0	AY	123.3	AZ	0.001	-					
	IX	789.3	IY	197.3	IZ	16884.3						
'D-8'	AX	136.0	AY	113.3	AZ	0.001	-					
	IX	725.3	IY	181.3	IZ	13101.3						
'D.5-1'	AX	64.0	AY	53.3	AZ	0.001	-					
	IX	341.3	IY	85.3	IZ	1365.3						
'D.5-2'	AX	152.0	AY	126.7	AZ	0.001	-					
	IX	810.7	IY	202.7	IZ	18290.7						
'E-1'	AX	248.0	AY	199.3	AZ	0.001	-					
	IX	1152.0	IY	288.0	IZ	52488.0						
'E-2'	AX	613.0	AY	510.8	AZ	0.001	IX	3269.3	IY	817.3	IZ	1199720.8
'E-a'	AX	214.0	AY	178.3	AZ	0.001	IX	1141.3	IY	285.3	IZ	51043.5
'E-b'	AX	320.0	AY	266.7	AZ	0.001	IX	1706.7	IY	426.7	IZ	170666.7
'E-3'	AX	607.0	AY	471.1	AZ	0.001	-					
	IX	2714.7	IY	678.7	IZ	1164836.2						
'E-4'	AX	455.3	AY	379.4	AZ	0.001	-					
	IX	1365.8	IY	341.4	IZ	873627.1						
'F-1'	AX	248.0	AY	175.3	AZ	0.001	-					
	IX	938.7	IY	234.7	IZ	79442.7						
'F-2'	AX	418.0	AY	340.1	AZ	0.001	-					
	IX	2112.0	IY	528.0	IZ	323433.0						
'G-1'	AX	248.0	AY	175.3	AZ	0.001	-					
	IX	938.7	IY	234.7	IZ	79442.7						
'G-2'	AX	612.0	AY	510.0	AZ	0.001	-					
	IX	3264.0	IY	816.0	IZ	1193859.0						
'G-3'	AX	281.0	AY	234.2	AZ	0.001	-					
	IX	1498.7	IY	374.7	IZ	115562.7						
'G-4'	AX	409.0	AY	327.4	AZ	0.001	-					
	IX	1936.0	IY	484.0	IZ	249125.8						
'G-5'	AX	409.0	AY	340.8	AZ	0.001	-					
	IX	2181.3	IY	545.3	IZ	356343.4						
'H-1'	AX	248.0	AY	199.3	AZ	0.001	-					
	IX	1152.0	IY	288.0	IZ	52488.0						
'H-2'	AX	610.0	AY	500.1	AZ	0.001	-					
	IX	3136.0	IY	784.0	IZ	1058841.0						
'H-3'	AX	112.0	AY	93.3	AZ	0.001	-					
	IX	597.3	IY	149.3	IZ	7317.3						
'H-4'	AX	157.5	AY	110.9	AZ	0.001	-					
	IX	319.5	IY	79.9	IZ	11184.7						
'H-5'	AX	112.0	AY	93.3	AZ	0.001	-					
	IX	597.3	IY	149.3	IZ	7317.3						
'H-6'	AX	157.5	AY	131.3	AZ	0.001	-					
	IX	472.5	IY	118.1	IZ	36175.8						
'H.75-1'	AX	248.0	AY	199.3	AZ	0.001	-					
	IX	1152.0	IY	288.0	IZ	52488.0						
'J-1'	AX	100.0	AY	83.3	AZ	0.001	-					
	IX	533.3	IY	133.3	IZ	5208.3						
'J-2'	AX	455.0	AY	379.2	AZ	0.001	IX	2426.7	IY	606.7	IZ	490606.1
'J-c'	AX	24.0	AY	20.0	AZ	0.001	IX	128.0	IY	32.0	IZ	72.0
'J-d'	AX	365.0	AY	304.2	AZ	0.001	IX	1946.7	IY	486.7	IZ	253266.3
'J-3'	AX	411.0	AY	332.2	AZ	0.001	-					
	IX	1936.0	IY	484.0	IZ	249125.8						
'J-4'	AX	411.0	AY	342.5	AZ	0.001	-					
	IX	2192.0	IY	548.0	IZ	361596.5						
'J-5'	AX	136.0	AY	113.3	AZ	0.001	IX	725.3	IY	181.3	IZ	13101.3
'J-a'	AX	68.0	AY	56.7	AZ	0.001	IX	362.7	IY	90.7	IZ	1637.7
'J-b'	AX	52.0	AY	43.3	AZ	0.001	IX	277.3	IY	69.3	IZ	732.3
'J-6'	AX	136.0	AY	113.3	AZ	0.001	-					
	IX	725.3	IY	181.3	IZ	13101.3						
'J-7'	AX	136.0	AY	113.3	AZ	0.001	-					
	IX	725.3	IY	181.3	IZ	13101.3						
'J.4-1'	AX	248.0	AY	175.3	AZ	0.001	-					
	IX	938.7	IY	234.7	IZ	79442.7						
'J.9-1'	AX	248.0	AY	175.3	AZ	0.001	-					
	IX	938.7	IY	234.7	IZ	79442.7						
'K-1'	AX	75.0	AY	62.5	AZ	0.001	-					
	IX	225.0	IY	56.3	IZ	3906.3						
'K-2'	AX	42.0	AY	35.0	AZ	0.001	-					
	IX	126.0	IY	31.5	IZ	686.0						

'K-3'	AX	105.0	AY	87.5	AZ	0.001	-						
	IX	315.0	IY	78.8	IZ	10718.8							
'K-4'	AX	303.8	AY	246.4	AZ	0.001	-						
	IX	816.8	IY	204.2	IZ	186844.3							
'K-5'	AX	303.8	AY	253.1	AZ	0.001	-						
	IX	911.3	IY	227.8	IZ	259492.7							
'K.5-1'	AX	248.0	AY	199.3	AZ	0.001	-						
	IX	1152.0	IY	288.0	IZ	52488.0							
'K.5-2'	AX	160.0	AY	122.4	AZ	0.001	-						
	IX	629.3	IY	157.3	IZ	8557.5							
'K.8-1'	AX	112.0	AY	93.3	AZ	0.001	-						
	IX	597.3	IY	149.3	IZ	7317.3							
'K.8-2'	AX	314.0	AY	261.7	AZ	0.001	-						
	IX	1674.7	IY	418.7	IZ	161245.5							
'L-1'	AX	611.0	AY	509.2	AZ	0.001	IX	3258.7	IY	814.7	IZ	1188016.3	
'L-a'	AX	167.0	AY	139.2	AZ	0.001	IX	890.7	IY	222.7	IZ	24257.6	
'L-b'	AX	364.0	AY	303.3	AZ	0.001	IX	1941.3	IY	485.3	IZ	251190.3	
'L-2'	AX	308.3	AY	250.5	AZ	0.001	-						
	IX	839.3	IY	209.8	IZ	202715.3							
'L-3'	AX	605.0	AY	504.2	AZ	0.001	-						
	IX	3226.7	IY	806.7	IZ	1153360.0							
'L-4'	AX	303.8	AY	247.1	AZ	0.001	-						
	IX	825.8	IY	206.4	IZ	193089.3							
'L-5'	AX	252.0	AY	210.0	AZ	0.001	-						
	IX	756.0	IY	189.0	IZ	148176.0							
'L-6'	AX	303.8	AY	237.6	AZ	0.001	-						
	IX	713.3	IY	178.3	IZ	124433.6							
'L-7'	AX	234.0	AY	195.0	AZ	0.001	-						
	IX	702.0	IY	175.5	IZ	118638.0							
'M-1'	AX	90.0	AY	75.0	AZ	0.001	-						
	IX	270.0	IY	67.5	IZ	6750.0							
'M-2'	AX	75.0	AY	62.5	AZ	0.001	-						
	IX	225.0	IY	56.3	IZ	3906.3							
'M-3'	AX	156.0	AY	130.0	AZ	0.001	-						
	IX	468.0	IY	117.0	IZ	35152.0							
'M.3-1'	AX	158.0	AY	131.7	AZ	0.001	-						
	IX	842.7	IY	210.7	IZ	20543.3							
'M.3-2'	AX	180.0	AY	139.9	AZ	0.001	-						
	IX	832.0	IY	208.0	IZ	19773.0							
'N-1'	AX	753.0	AY	627.5	AZ	0.001	IX	4016.0	IY	1004.0	IZ	2223738.4	
'N-a'	AX	307.0	AY	255.8	AZ	0.001	IX	1637.3	IY	409.3	IZ	150700.2	
'N-b'	AX	185.0	AY	154.2	AZ	0.001	IX	986.7	IY	246.7	IZ	32977.2	
'N-c'	AX	145.0	AY	120.8	AZ	0.001	IX	773.3	IY	193.3	IZ	15878.3	
'N-2'	AX	284.0	AY	236.7	AZ	0.001	-						
	IX	1514.7	IY	378.7	IZ	119303.7							
'N-3'	AX	100.0	AY	83.3	AZ	0.001	-						
	IX	533.3	IY	133.3	IZ	5208.3							
'N-4'	AX	455.0	AY	379.2	AZ	0.001	IX	2426.7	IY	606.7	IZ	490606.1	
'N-d'	AX	368.0	AY	306.7	AZ	0.001	IX	1962.7	IY	490.7	IZ	259562.7	
'N-e'	AX	59.0	AY	49.2	AZ	0.001	IX	314.7	IY	78.7	IZ	1069.7	
'N-5'	AX	605.0	AY	504.2	AZ	0.001	-						
	IX	3226.7	IY	806.7	IZ	1153360.0							
'N-6'	AX	949.0	AY	853.2	AZ	0.001	-						
	IX	5061.3	IY	1265.3	IZ	2034994.1							
'N-7'	AX	175.0	AY	145.8	AZ	0.001	-						
	IX	933.3	IY	233.3	IZ	27913.4							
'N-8'	AX	1109.0	AY	924.2	AZ	0.001	-						
	IX	5914.7	IY	1478.7	IZ	7103843.9							
'O-1'	AX	619.0	AY	515.8	AZ	0.001	IX	3301.3	IY	825.3	IZ	1235295.1	
'O-a'	AX	177.0	AY	147.5	AZ	0.001	IX	944.0	IY	236.0	IZ	28881.4	
'O-b'	AX	262.0	AY	218.3	AZ	0.001	IX	1397.3	IY	349.3	IZ	93670.5	
'O-c'	AX	134.0	AY	111.7	AZ	0.001	IX	714.7	IY	178.7	IZ	12531.8	
'O-2'	AX	605.0	AY	504.2	AZ	0.001	IX	3226.7	IY	806.7	IZ	1153360.0	
'O-d'	AX	473.0	AY	394.2	AZ	0.001	IX	2522.7	IY	630.7	IZ	551165.7	
'O-e'	AX	100.0	AY	83.3	AZ	0.001	IX	533.3	IY	133.3	IZ	5208.3	
'O-3'	AX	455.0	AY	379.2	AZ	0.001	-						
	IX	2426.7	IY	606.7	IZ	490606.1							
'O-4'	AX	149.0	AY	107.2	AZ	0.001	-						
	IX	474.7	IY	118.7	IZ	3671.7							
'O-5'	AX	1593.0	AY	1312.9	AZ	0.001	-						
	IX	8112.0	IY	2028.0	IZ	21054556.5							
'O-6'	AX	1293.0	AY	1077.5	AZ	0.001	-						
	IX	6896.0	IY	1724.0	IZ	11258858.1							
'P-1'	AX	348.8	AY	290.6	AZ	0.001	IX	1046.3	IY	261.6	IZ	392752.4	
'P-a'	AX	43.5	AY	36.3	AZ	0.001	IX	130.5	IY	32.6	IZ	762.2	
'P-b'	AX	196.5	AY	163.8	AZ	0.001	IX	589.5	IY	147.4	IZ	70252.8	
'P-c'	AX	63.0	AY	52.5	AZ	0.001	IX	189.0	IY	47.3	IZ	2315.3	
'R-1'	AX	928.5	AY	773.8	AZ	0.001	IX	11142.0	IY	2785.5	IZ	1852942.6	
'R-a'	AX	139.5	AY	116.3	AZ	0.001	IX	1674.0	IY	418.5	IZ	6284.0	
'R-b'	AX	505.5	AY	421.3	AZ	0.001	IX	6066.0	IY	1516.5	IZ	299005.9	
'R-c'	AX	193.5	AY	161.3	AZ	0.001	IX	2322.0	IY	580.5	IZ	16771.0	
'R-2'	AX	906.0	AY	755.0	AZ	0.001	IX	10872.0	IY	2718.0	IZ	1721475.5	
'R-d'	AX	198.0	AY	165.0	AZ	0.001	IX	2376.0	IY	594.0	IZ	17968.5	
'R-e'	AX	408.0	AY	340.0	AZ	0.001	IX	4896.0	IY	1224.0	IZ	157216.0	
'R-f'	AX	150.0	AY	125.0	AZ	0.001	IX	1800.0	IY	450.0	IZ	7812.5	
'R-3'	AX	682.5	AY	568.8	AZ	0.001	-						

	IX	8190.0	IY	2047.5	IZ	735909.2	
'R-4'	AX	2009.3	AY	1664.5	AZ	0.001	-
	IX	13228.3	IY	3307.1	IZ	33380716.7	
'R-5'	AX	1339.5	AY	1062.4	AZ	0.001	-
	IX	3919.5	IY	979.9	IZ	22253811.2	
'dummy 1'	AX	0.001	AY	0.001	AZ	0.001	-
	IX	0.001	IY	0.001	IZ	0.001	-
'dummy 2'	AX	0.001	AY	0.001	AZ	0.001	-
	IX	0.001	IY	0.001	IZ	0.001	-
'dummy 3'	AX	0.001	AY	0.001	AZ	0.001	-
	IX	0.001	IY	0.001	IZ	0.001	-
'dummy 4'	AX	0.001	AY	0.001	AZ	0.001	-
	IX	0.001	IY	0.001	IZ	0.001	-

\$

TYPE	RIGID	SOLID	
RIGID	BODY	INCIDENCES	

100 EXISTING 4 6 TO 12 14 TO 18 21 24 TO 26 29 30 31 33 35 39 41 42 44 TO 47 49 TO 52 -

54 TO 61 63 65 66 69 70 74 78 TO 87 99 1000 TO 1076 MASTER 100 \$ Base slab

200 EXISTING 101 TO 187 201 TO 238 199 MASTER 200 \$ EL. 31.5

400 301 TO 338 401 TO 429 399 MASTER 400 \$ EL. 65.5

600 501 TO 529 601 TO 604 599 MASTER 600 \$ EL. 99.5

700 701 TO 704 MASTER 700 \$ EL. 106.5

\$

1	2000 TO 2005	MASTER	1	\$ WALL 1.0
2	2006 TO 2010	MASTER	2	\$ WALL 3.0
3	2011 TO 2015	MASTER	3	\$ WALL 3.5
4	2016 TO 2017	MASTER	5	\$ WALL 4.0
5	2018 TO 2019	MASTER	13	\$ WALL 5.0
6	2020 TO 2021	MASTER	19	\$ WALL 8.3
7	2022 TO 2024	MASTER	20	\$ WALL 9.0
8	2025 TO 2028	MASTER	22	\$ WALL 10.0
9	2029 TO 2031	MASTER	23	\$ WALL 10.0
10	2032 TO 2033	MASTER	27	\$ WALL 11.0
11	2034 TO 2035	MASTER	28	\$ WALL 11.0
12	2036 TO 2037	MASTER	32	\$ WALL 12.0
13	2038 TO 2039	MASTER	34	\$ WALL 13.0
14	2040 TO 2041	MASTER	36	\$ WALL 13.0
15	2042 TO 2043	MASTER	37	\$ WALL 13.0

\$

16	2044 TO 2046	MASTER	38	\$ WALL A.0
17	2047 TO 2049	MASTER	40	\$ WALL D.0
18	2050 TO 2051	MASTER	43	\$ WALL E.0
19	2052 TO 2053	MASTER	48	\$ WALL J.0
20	2054 TO 2055	MASTER	53	\$ WALL J.0
21	2056 TO 2057	MASTER	62	\$ WALL L.0
22	2058 TO 2060	MASTER	68	\$ WALL N.0
23	2061 TO 2062	MASTER	71	\$ WALL N.0
24	2063 TO 2065	MASTER	72	\$ WALL O.0
25	2066 TO 2067	MASTER	73	\$ WALL O.0
26	2068 TO 2070	MASTER	75	\$ WALL P.0
27	2071 TO 2073	MASTER	76	\$ WALL R.0
28	2074 TO 2076	MASTER	77	\$ WALL R.0

\$

INERTIA OF JOINTS WEIGHT GRAVITY 32.2

99	TRANS X	366043.3 Y	366043.3 Z	366043.3 \$ Base Slab Mass
199	TRANS X	230658.4 Y	230658.4 Z	230658.4 \$ Mass at 31.5
399	TRANS X	174027.9 Y	174027.9 Z	174027.9 \$ Mass at 65.5
599	TRANS X	110761.4 Y	110761.4 Z	110761.4 \$ Mass at 99.5
700	TRANS X	6098.0 Y	6098.0 Z	6098.0 \$ Mass at 106.5

\$

INERTIA OF JOINTS MASS

99	ROT X	2.04E+08 Y	1.79E+08 Z	3.82E+08 \$ Mass Moment of Inertia at 0.0
199	ROT X	1.18E+08 Y	1.07E+08 Z	2.25E+08 \$ Mass Moment of Inertia at 31.5
399	ROT X	9.55E+07 Y	8.45E+07 Z	1.80E+08 \$ Mass Moment of Inertia at 65.5
599	ROT X	6.55E+07 Y	5.29E+07 Z	1.18E+08 \$ Mass Moment of Inertia at 99.5
700	ROT X	8.27E+05 Y	1.07E+05 Z	9.33E+05 \$ Mass Moment of Inertia at 106.5

\$

STATUS SUPPORT JOINTS 100

UNITS RADIANS

JOINT RELEASES

\$ LOWER BOUND 35 ALLUVIUM SOIL SPRINGS

\$100	KFX	1.65E+07 KFY	1.74E+07 KFZ	2.01E+07 -
\$	KMX	1.23E+12 KMY	9.86E+11 KMZ	1.45E+12

\$ MEDIAN 35 ALLUVIUM SOIL SPRINGS

\$100	KFX	3.71E+07 KFY	3.90E+07 KFZ	4.50E+07 -
\$	KMX	2.75E+12 KMY	2.21E+12 KMZ	3.25E+12

\$ UPPER BOUND 35 ALLUVIUM SPRINGS

\$100	KFX	7.68E+07 KFY	8.09E+07 KFZ	9.33E+07 -
\$	KMX	5.71E+12 KMY	4.58E+12 KMZ	6.74E+12

\$ LOWER BOUND 110 ALLUVIUM SPRINGS

\$100	KFX	1.23E+07 KFY	1.30E+07 KFZ	1.50E+07 -
\$	KMX	9.15E+11 KMY	7.34E+11 KMZ	1.08E+12

\$ MEDIAN 110 ALLUVIUM SOIL SPRINGS

\$100	KFX	2.93E+07 KFY	3.09E+07 KFZ	3.56E+07 -
\$	KMX	2.18E+12 KMY	1.75E+12 KMZ	2.57E+12

\$ UPPER BOUND 110 ALLUVIUM SOIL SPRINGS

```
$100      KFX      6.87E+07 KFY      7.24E+07 KPZ      8.35E+07 -
$         KMX      5.11E+12 KMY      4.10E+12 KMZ      6.03E+12
$
LOADING 1 'LUMPED JOINT DEAD LOAD -Z VERTICAL DIRECTION'
JOINT LOAD
99        FORCE     Z      -366043.3
199       FORCE     Z      -230658.4
399       FORCE     Z      -174027.9
599       FORCE     Z      -110761.4
700       FORCE     Z      -6098.0
$
UNITS     CYCLES
EIGEN PARAMETERS
SOLVE USING GTLANCZOS
FREQUENCY SPECIFICATIONS 0.0 TO 100.0
PRINT MAX
END
PERFORM ASSEMBLY FOR DYNAMICS
PERFORM EIGENVALUE ANALYSIS
$ LIST DYNAMIC EIGENVALUES
LIST DYNAMIC PARTICIPATION FACTORS
LIST DYNAMIC MASS SUMMARY
$
INACTIVE MEMBERS 100 200 400 600 700 1 TO 28
$
$         5e-4 Point D/E Horizontal 20% Damped Seismic Design Response Spectrum
$         Frequency(Hz) Spectral Acceleration (g)
$
UNITS     FEET     SECONDS CYCLES
$ 20% CRITICAL DAMPING for the first three modes
STORE RESPONSE SPECTRUM ACCELERATION LOG VS NATURAL FREQUENCY LOG 'HORIZ'

DAMPING RATIO 0.07 FACTOR 32.17
0.0101 0.10
0.0405 0.20
0.0567 0.250
0.0869 0.33
0.1503 0.50
0.2151 0.67
0.3525 1.00
0.4310 1.18
0.4988 1.33
0.6463 1.67
0.7451 2.00
0.7927 2.17
0.8731 2.50
0.9068 2.78
0.9684 3.33
1.0325 4.17
1.0606 5.00
1.0862 5.88
1.1075 6.67
1.1273 8.33
1.1489 10.00
1.1615 11.11
1.1318 13.33
1.0854 16.67
1.0399 20.00
0.9562 25.00
0.8589 33.33
0.7287 50.00
0.5802 100.00
DAMPING RATIO 0.20 FACTOR 32.17
0.0073 0.10
0.0292 0.20
0.0401 0.250
0.0603 0.33
0.1021 0.50
0.1448 0.67
0.2359 1.00
0.2884 1.18
0.3339 1.33
0.4327 1.67
0.4988 2.00
0.5307 2.17
0.5845 2.50
0.6071 2.78
0.6483 3.33
0.6912 4.17
0.7100 5.00
0.7272 5.88
0.7535 6.67
0.7855 8.33
0.8307 10.00
0.8579 11.11
0.8670 13.33
```

```
0.8697 16.67
0.8646 20.00
0.8315 25.00
0.7947 33.33
0.7287 50.00
0.5802 100.00
END OF RESPONSE SPECTRUM
$
$      5e-4 Point D/E Vertical 20% Damped Seismic Design Response Spectrum
$
$      Frquency(Hz) Spectral Acceleration (g)
$
$ 20% CRITICAL DAMPING for the first three modes
STORE RESPONSE SPECTRUM ACCELERATION LOG VS NATURAL FREQUENCY LOG 'VERT'

DAMPING RATIO 0.07 FACTOR 32.17
0.0100 0.10
0.0328 0.20
0.0432 0.25
0.0616 0.33
0.0937 0.50
0.1227 0.67
0.1762 1.00
0.2033 1.18
0.2271 1.33
0.2775 1.67
0.3282 2.00
0.3545 2.17
0.4031 2.50
0.4401 2.78
0.5112 3.33
0.6125 4.17
0.6943 5.00
0.7657 5.88
0.8271 6.67
0.8782 8.33
0.9009 10.00
0.9176 11.11
0.9465 13.33
0.9263 16.67
0.9013 20.00
0.8659 25.00
0.7946 33.33
0.7126 50.00
0.5188 100.00
DAMPING RATIO 0.20 FACTOR 32.17
0.0072 0.10
0.0234 0.20
0.0301 0.25
0.0419 0.33
0.0622 0.50
0.0805 0.67
0.1148 1.00
0.1324 1.18
0.1479 1.33
0.1808 1.67
0.2139 2.00
0.2310 2.17
0.2627 2.50
0.2868 2.78
0.3331 3.33
0.3960 4.17
0.4444 5.00
0.4848 5.88
0.5219 6.67
0.5577 8.33
0.5787 10.00
0.6014 11.11
0.6402 13.33
0.6486 16.67
0.6508 20.00
0.6481 25.00
0.6548 33.33
0.7126 50.00
0.5188 100.00
END OF RESPONSE SPECTRUM
$
$ DAMPING RATIOS 0.20 3, 0.07 27
$
$ RESPONSE SPECTRUM LOADING 'HX' 'GLOBAL X DIRECTION SPECTRA'
$      SUPPORT ACCELERATIONS
$      TRANSLATION X FILE 'HORIZ'
END RESPONSE SPECTRA LOAD
$
$ RESPONSE SPECTRUM LOADING 'HY' 'GLOBAL Y DIRECTION SPECTRA'
$      SUPPORT ACCELERATIONS
```

```
TRANSLATION Y FILE 'HORIZ'
END RESPONSE SPECTRA LOAD
$
RESPONSE SPECTRUM LOADING 'VZ' 'GLOBAL Z DIRECTION SPECTRA'
SUPPORT ACCELERATIONS
TRANSLATION Z FILE 'VERT'
END RESPONSE SPECTRA LOAD
$
PERFORM RESPONSE SPECTRA ANALYSIS
$
COMPUTE RESPONSE SPECTRUM ACCELERATIONS MODAL COMBINATION NRC TPM NODES ALL

$
COMPUTE RESPONSE SPECTRA FORCES MODAL COMBINATION NRC TPM MEMBERS ALL BUT 100 200 400 600 700 1 TO 28

$
COMPUTE RESPONSE SPECTRUM DISPLACEMENTS MODE COMBINATION NRC TPM NODES ALL

$
LIST RESPONSE SPECTRA ACCELERATIONS MODAL COMBINATIONS NRC TPM NODES ALL

$
LIST RESPONSE SPECTRUM FORCES MODAL COMBINATION NRC TPM MEMBERS ALL BUT 100 200 400 600 700 1 TO 28

$
CREATE PSEUDO STATIC LOAD 'NRCTPM_X' FROM NRC TPM OF LOADING 'HX'
CREATE PSEUDO STATIC LOAD 'NRCTPM_Y' FROM NRC TPM OF LOADING 'HY'
CREATE PSEUDO STATIC LOAD 'NRCTPM_Z' FROM NRC TPM OF LOADING 'VZ'
$
CREATE LOADING COMBINATION 'SRSS_XYZ' TYPE RMS SPEC 'NRCTPM_X' 1.0 'NRCTPM_Y' 1.0 'NRCTPM_Z' 1.0

$
OUTPUT DECIMAL 1
$
LOAD LIST 'SRSS_XYZ'
LIST FORCES MEMBERS EXISTING
$
$ LIST RESPONSE SPECTRA DISPLACEMENTS FOR CALCULATING SUPPORT SPRING REACTIONS

$ MAGNITUDE OF THE DISPLACEMENT/ROTATION TIMES THE SUPPORT SPRING CONSTANT

$
OUTPUT DECIMAL 10
UNITS RADIANS
$ LIST DISPLACEMENTS JOINTS EXISTING 100
$ LOAD LIST ALL
LOAD LIST 'HX' 'HY' 'VZ'
OUTPUT MODAL CONTRIBUTIONS OFF
LIST RESPONSE SPECTRUM DISPLACEMENTS MODE COMBINATION NRC TPM JOINTS -

EXISTING 100
$
OUTPUT DECIMAL 1
$
LOAD LIST 1
STIFFNESS ANALYSIS
$
LIST FORCES MEMBERS EXISTING
$
OUTPUT DECIMAL 10
$
$ LIST STATIC DISPLACEMENTS FOR CALCULATING SUPPORT SPRING REACTIONS

$ MAGNITUDE OF THE DISPLACEMENT/ROTATION TIMES THE SUPPORT SPRING CONSTANT

$
LIST DISPLACEMENTS JOINTS EXISTING 100
$
```



## 8. RESULTS

The primary outputs of this calculation are:

- All mode shapes between 0.0 and 100.0 hertz
- Mass participation factors for all modes below 100.0 hertz
- Response spectra accelerations
- Response spectra forces for each global direction
- Response spectra forces combined using SRSS
- Dynamic spring displacements
- Dead load forces (includes 25% of the applied live load)
- Static spring displacements

In subsequent calculations, the inertial seismic forces (using the SRSS combination), dead load forces, and nodal accelerations will be used to do preliminary design of the concrete shear walls and diaphragms. There are 27 modes below 100 hertz providing 100% mass participation with no missing modes. The spring support displacements are used to obtain the global support reactions by multiplying each spring displacement or rotation by the corresponding spring constant. A subsequent calculation will use these spring reactions to determine the dynamic soil pressure under the basemat for preliminary design.

The outputs are reasonable based on the inputs. The forces and accelerations increase, as expected, with each increment increase of soil spring stiffness used (e.g. lower bound springs produce lowest forces, upper bound spring yields highest forces).

The outputs are also bounding with respect to their usage. The output used in all subsequent calculations will be based on the upper bound 35 spring support boundary condition. Coupled with the 20% damped spectral accelerations, the upper bound 35 spring support yields the highest (i.e. the most conservative) member forces, nodal accelerations and support displacements, and is considered appropriate for further Tier 1 analysis and design.

## 9. REFERENCES

BSC (Bechtel SAIC Company) 2003. *Q-List*. TDR-MGR-RL-000005 REV 00. Las Vegas, Nevada: Bechtel SAIC Company. ACC: DOC.20030930.0002.

BSC (Bechtel SAIC Company) 2003. *Users Manual: GT STRUDL Version 26*. 10829-UM-26-00. Las Vegas, Nevada: Bechtel SAIC Company. ACC: MOL.20030521.0191.

BSC (Bechtel SAIC Company) 2004. *Dry Transfer Facility Soil Springs*. 110-CYC-CY00-00100-000-00A. Las Vegas, Nevada: Bechtel SAIC Company. ACC: ENG.20040330.0006.

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MO0402SDSTMHIS.004. Seismic Design Spectra and Time Histories for the Surface Facilities Area (Point D/E) at 5E-4 Annual Exceedance Frequency.

DOE (U.S. Department of Energy) 2004. *Quality Assurance Requirements and Description*. DOE/RW-0333P, Rev. 14. Washington, D.C.: U.S. Department of Energy, Office of Civilian Radioactive Waste Management. ACC: DOC.20040331.0004.

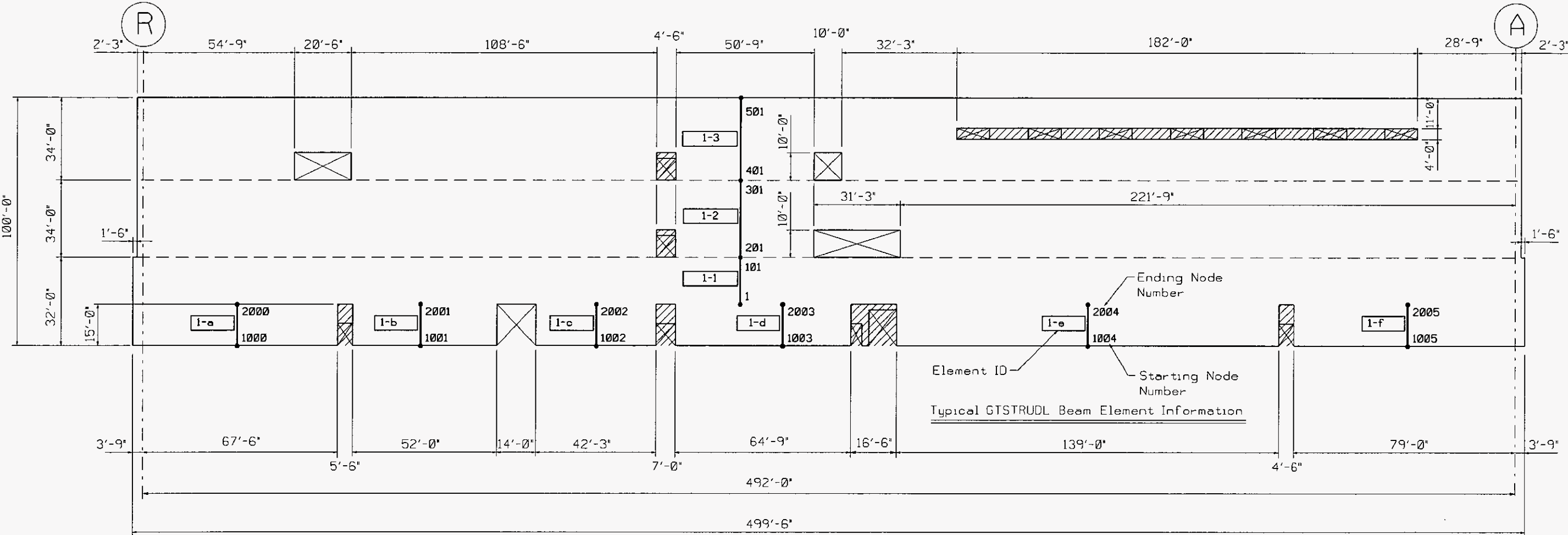
## **10. ATTACHMENTS**

1. GTSTRUDL Output using fixed base boundary condition (CD-ROM)	92
2. GTSTRUDL Output using lower bound 35 soil springs (CD-ROM)	103
3. GTSTRUDL Output using median 35 soil springs (CD-ROM)	103
4. GTSTRUDL Output using upper bound 35 soil springs (CD-ROM)	103
5. GTSTRUDL Output using lower bound 110 soil springs (CD-ROM)	103
6. GTSTRUDL Output using median 110 soil springs (CD-ROM)	103
7. GTSTRUDL Output using upper bound 110 soil springs (CD-ROM)	103
8. Dry Transfer Facility Wall Elevations Beam Stick Model Joints / Elements	32
9. Dry Transfer Facility General Arrangements	1

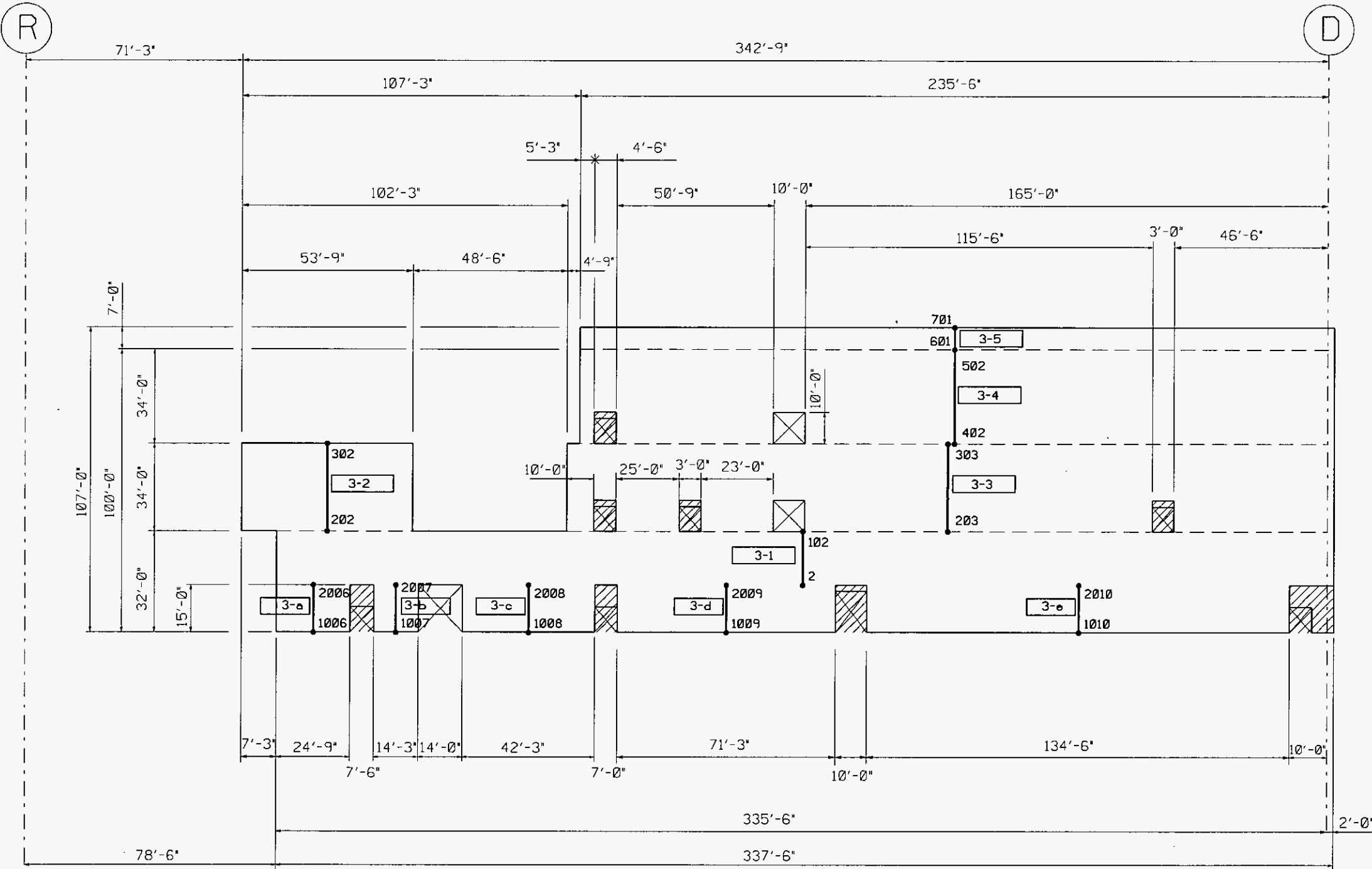
Attachments 1 through 7 are supplied on a CD-ROM for review. The filenames are as follows:

Attachment 1\_GTSTRUDL Output using fixed base boundary condition.doc  
Attachment 2\_GTSTRUDL Output using lower bound 35 soil springs.doc  
Attachment 3\_GTSTRUDL Output using median 35 soil springs.doc  
Attachment 4\_GTSTRUDL Output using upper bound 35 soil springs.doc  
Attachment 5\_GTSTRUDL Output using lower bound 110 soil springs.doc  
Attachment 6\_GTSTRUDL Output using median 110 soil springs.doc  
Attachment 7\_GTSTRUDL Output using upper bound 110 soil springs.doc

• ALL DIMENSIONS ARE +/- SIX INCHES

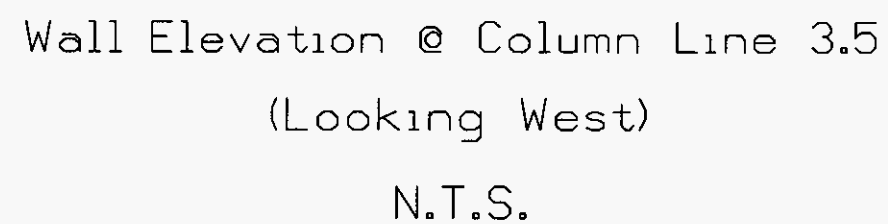


Wall Elevation @ Column Line 1.0  
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N.T.S.

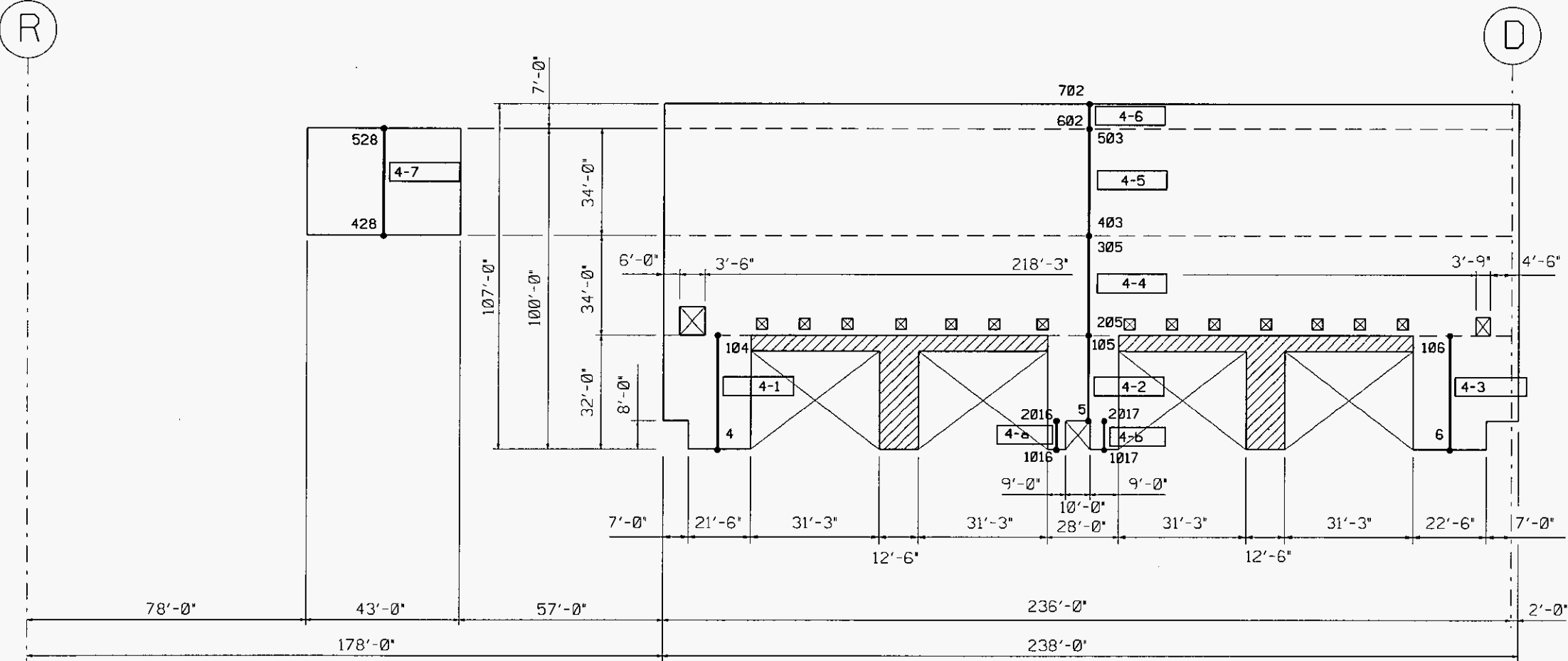


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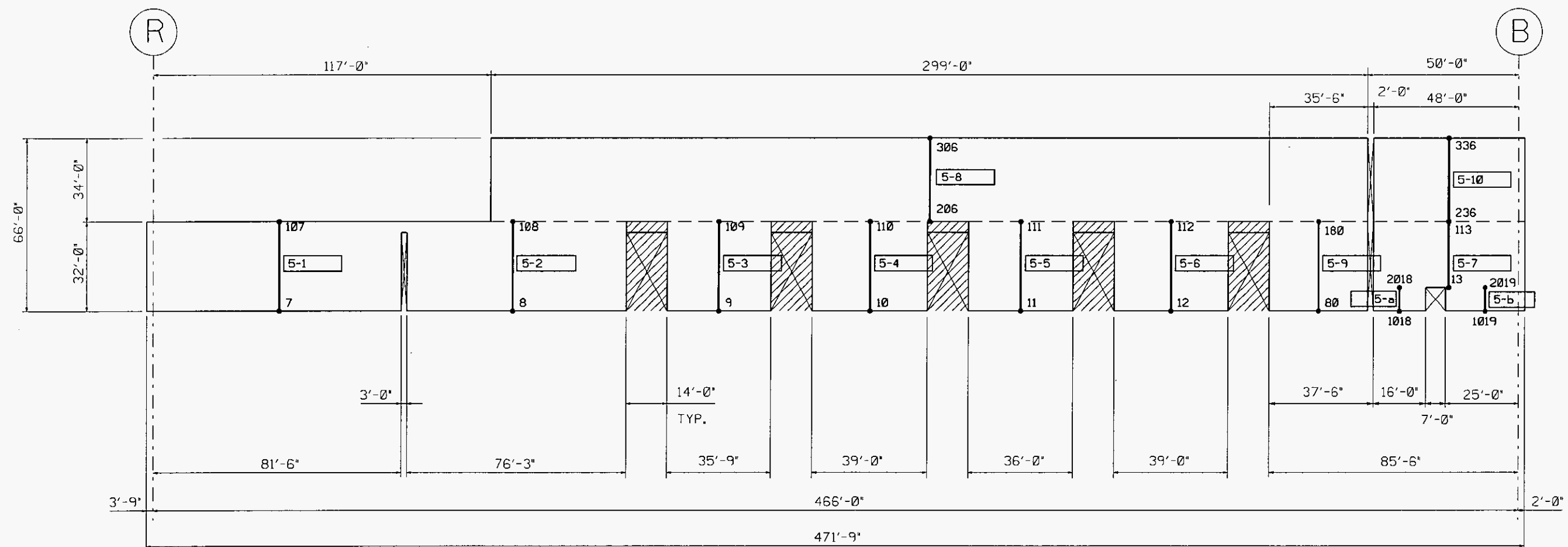
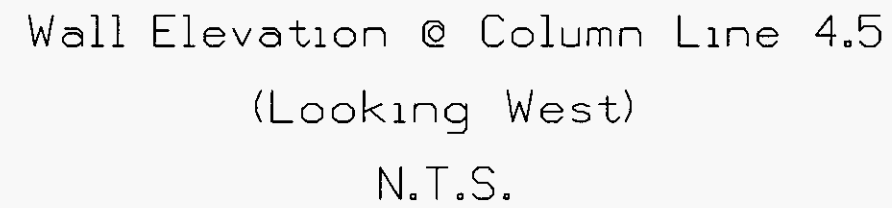
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• ALL DIMENSIONS ARE +/- SIX INCHES

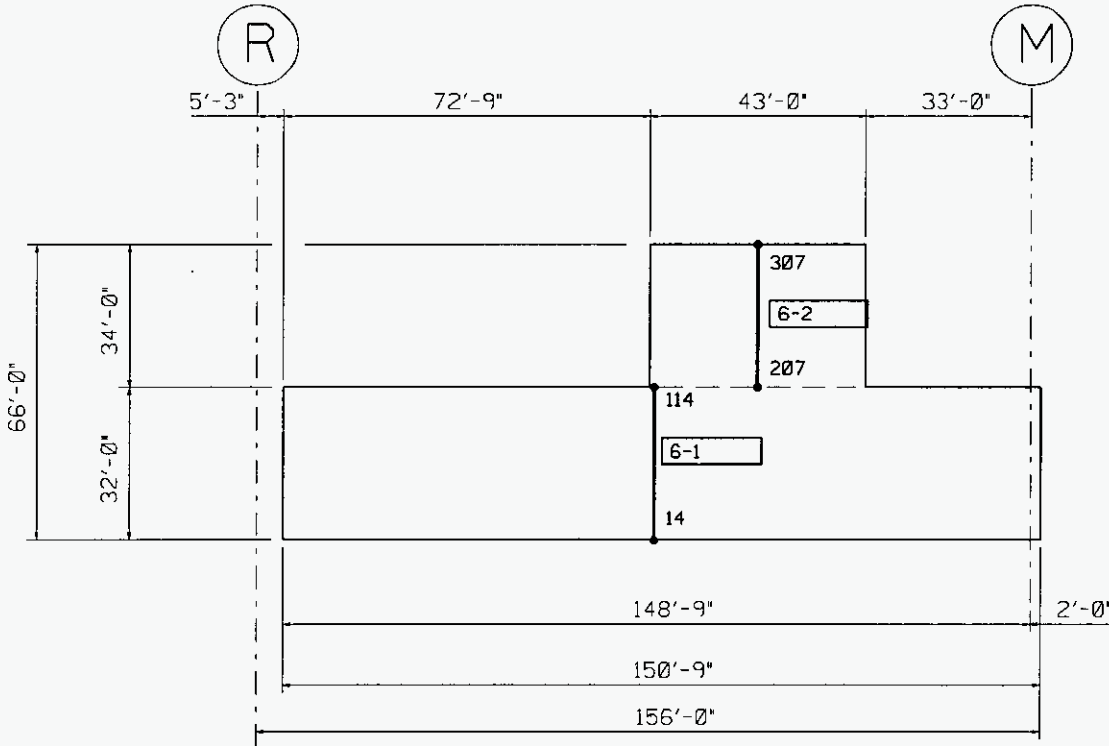


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N.T.S.



Wall Elevation @ Column Line 5.0  
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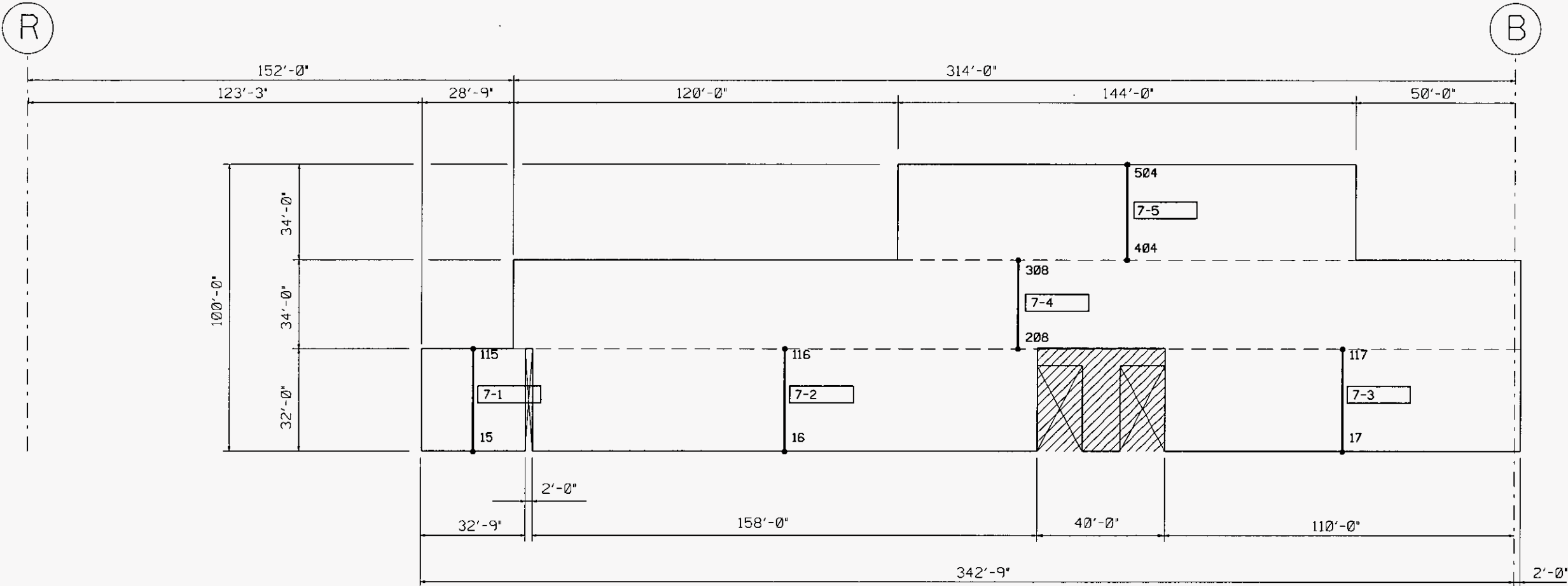
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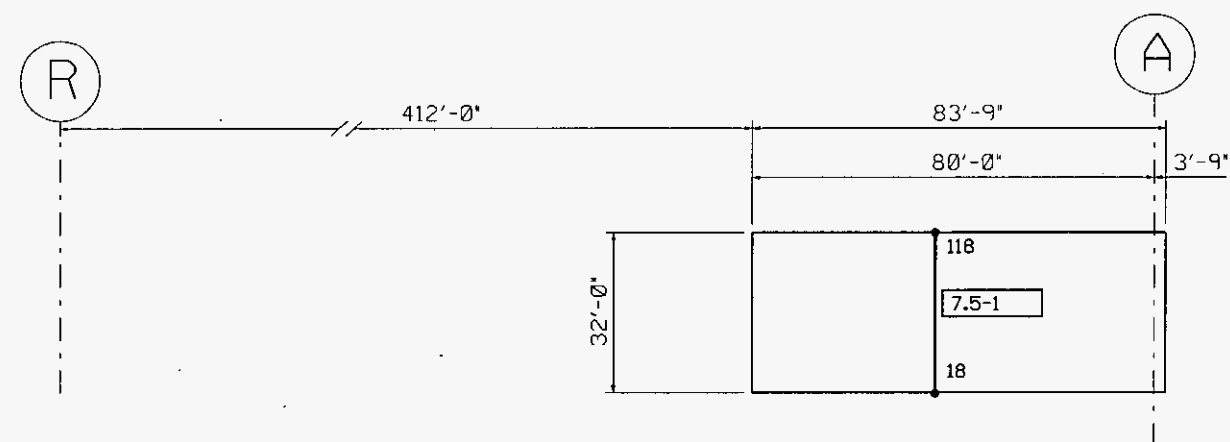


● ALL DIMENSIONS ARE +/- SIX INCHES

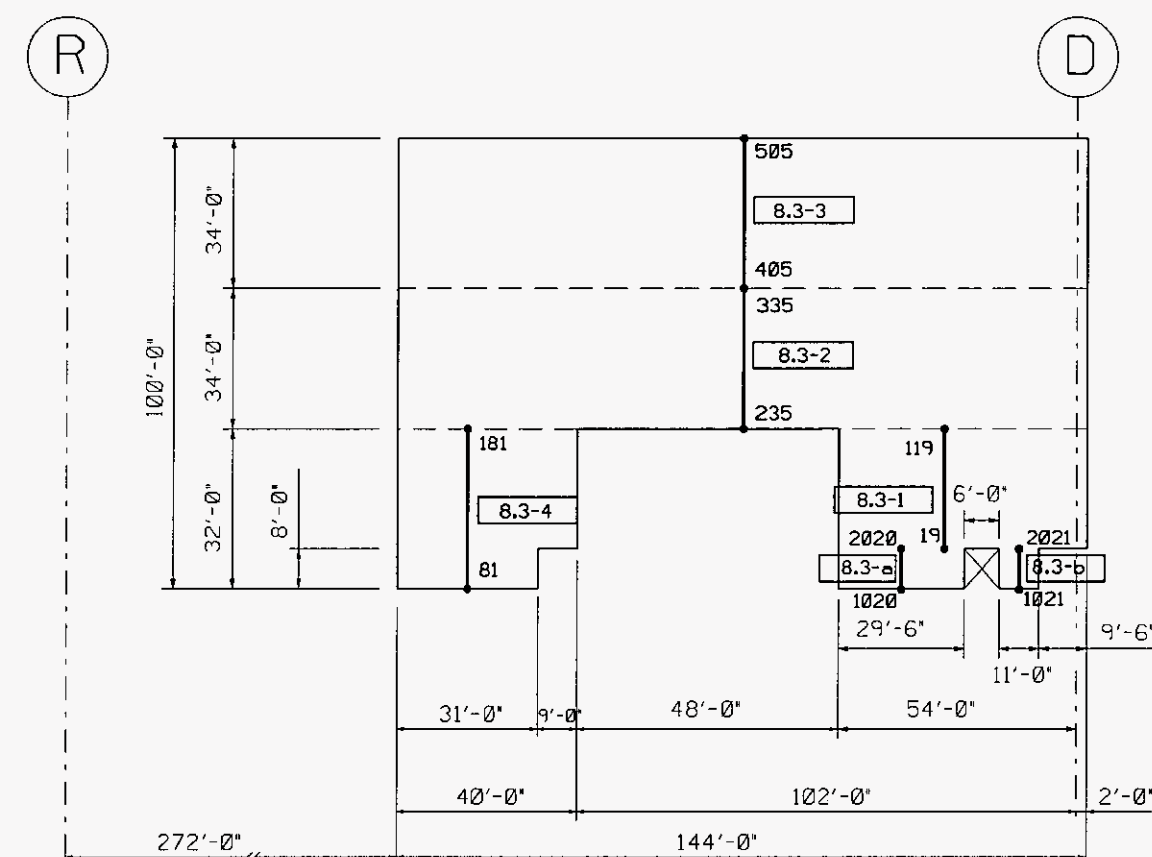


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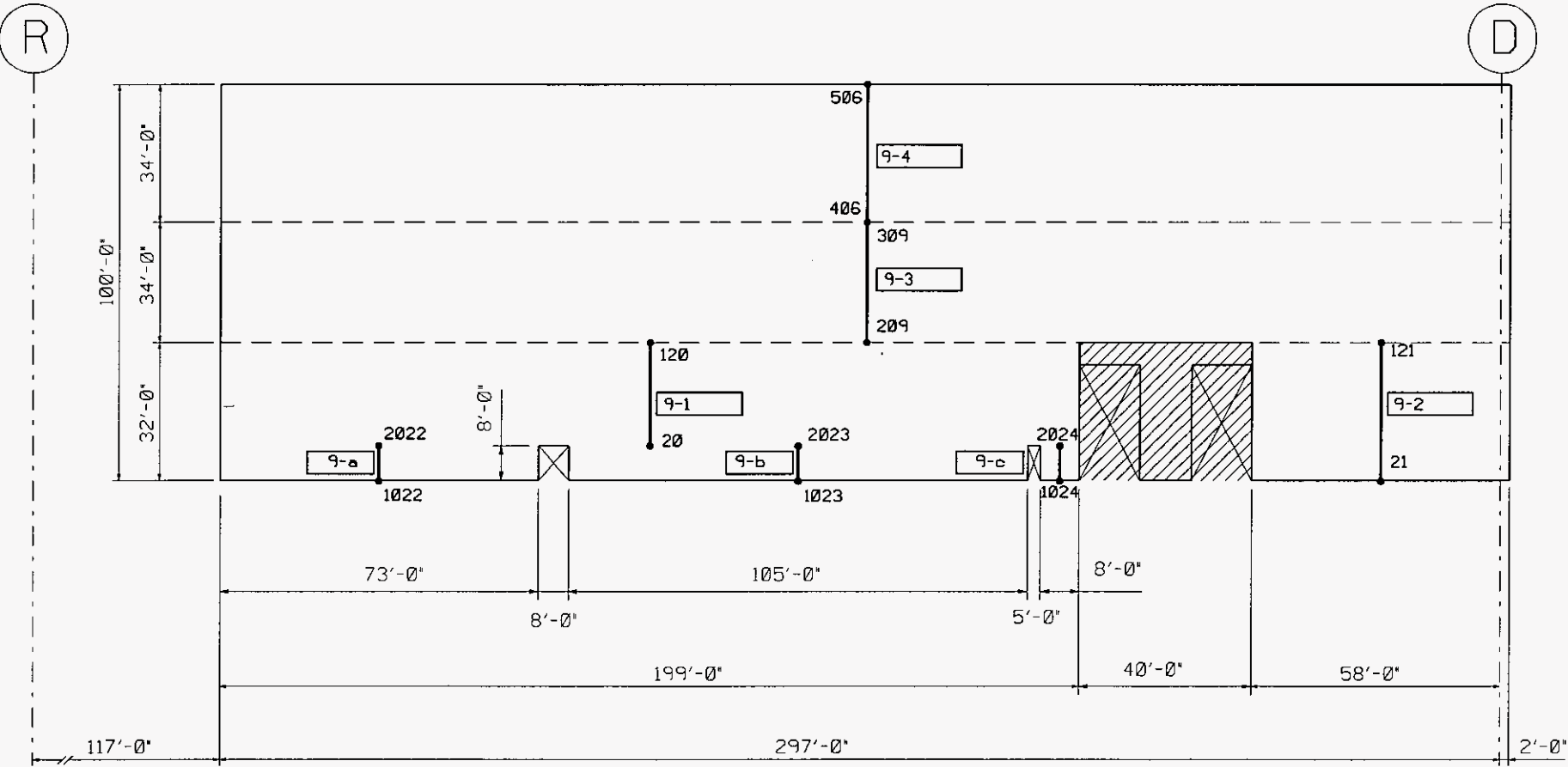
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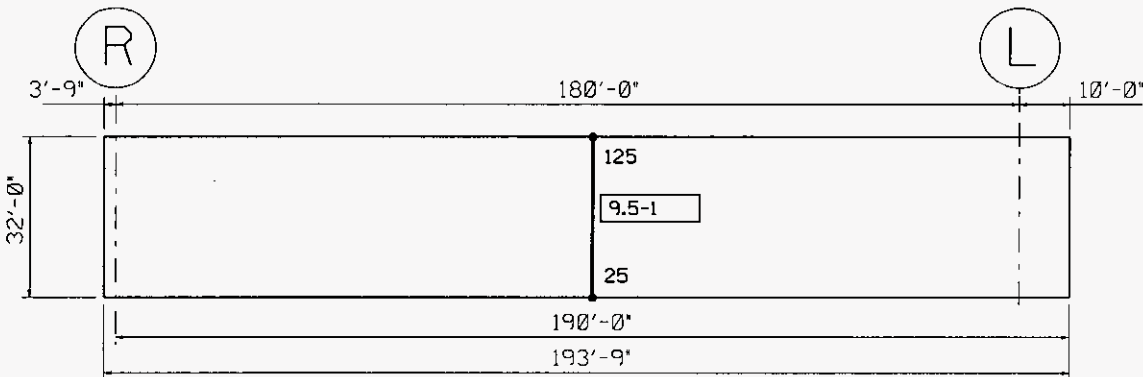


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(Looking West)  
N.T.S.



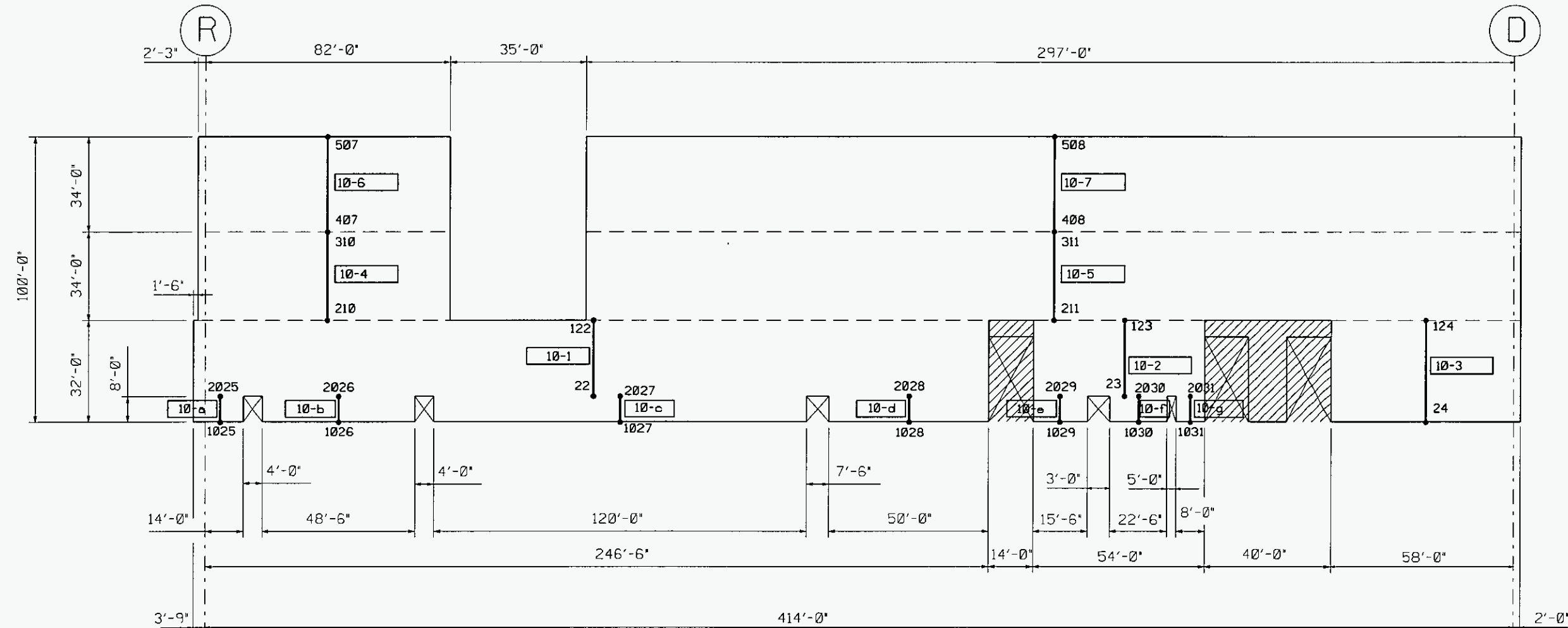
Wall Elevation @ Column Line 9.0  
(Looking West)  
N.T.S.

• ALL DIMENSIONS ARE +/- SIX INCHES



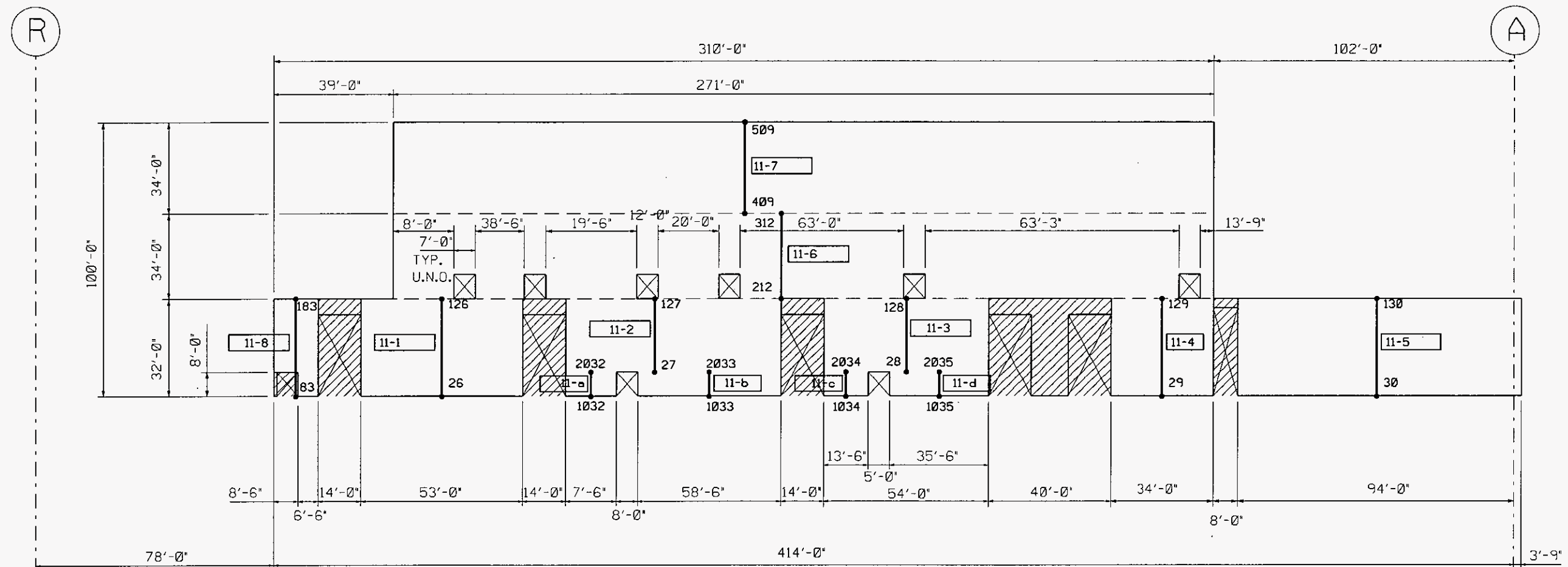
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• ALL DIMENSIONS ARE +/- SIX INCHES



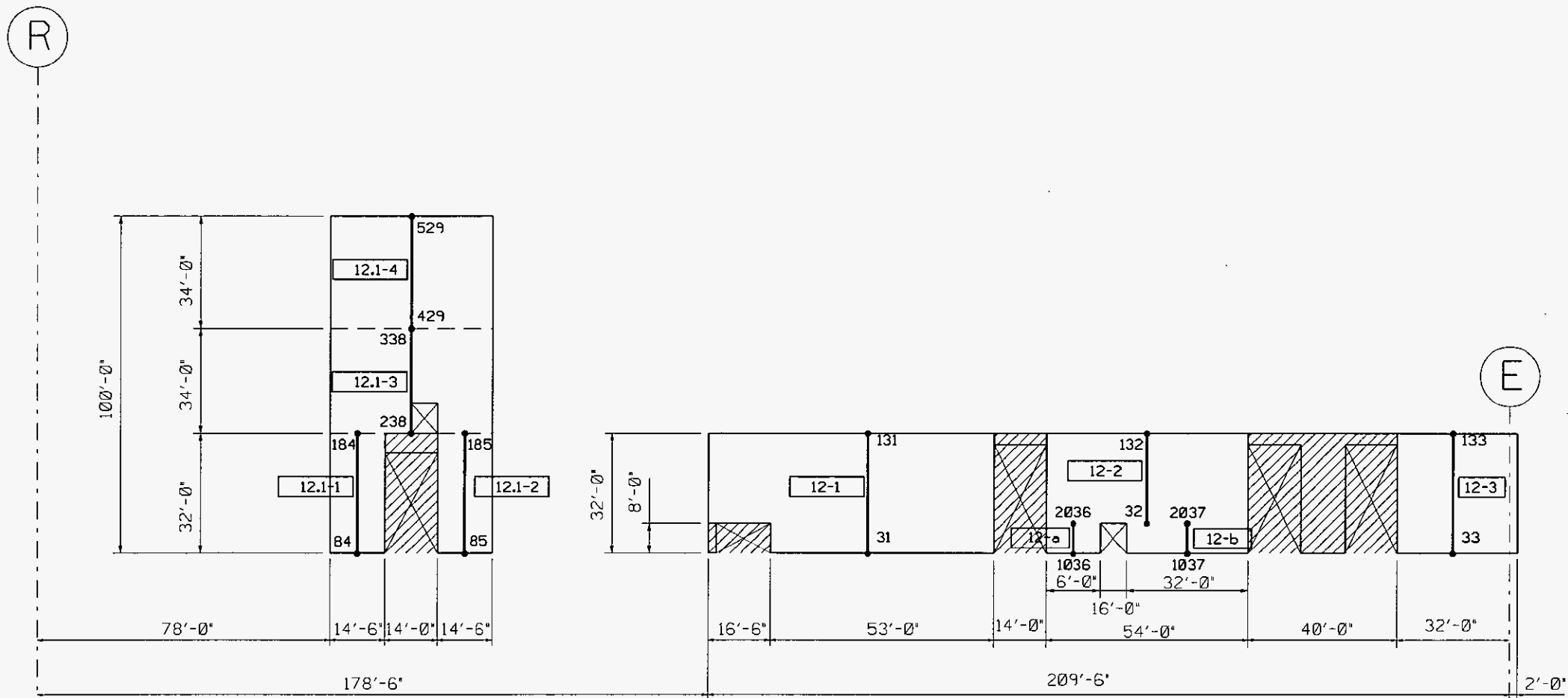
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(Looking West)  
N.T.S.

• ALL DIMENSIONS ARE +/- SIX INCHES



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(Looking West)  
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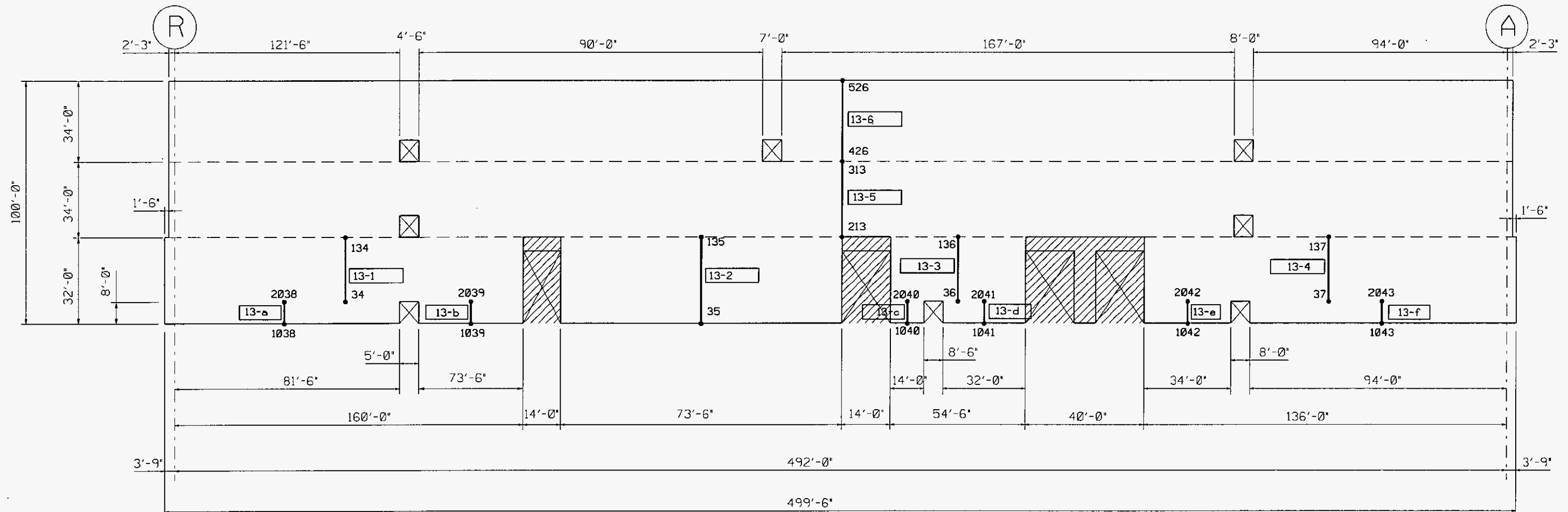
• ALL DIMENSIONS ARE +/- SIX INCHES



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(Looking West)  
N.T.S.

Wall Elevation @ Column Line 12.0  
(Looking West)  
N.T.S.

• ALL DIMENSIONS ARE +/- SIX INCHES

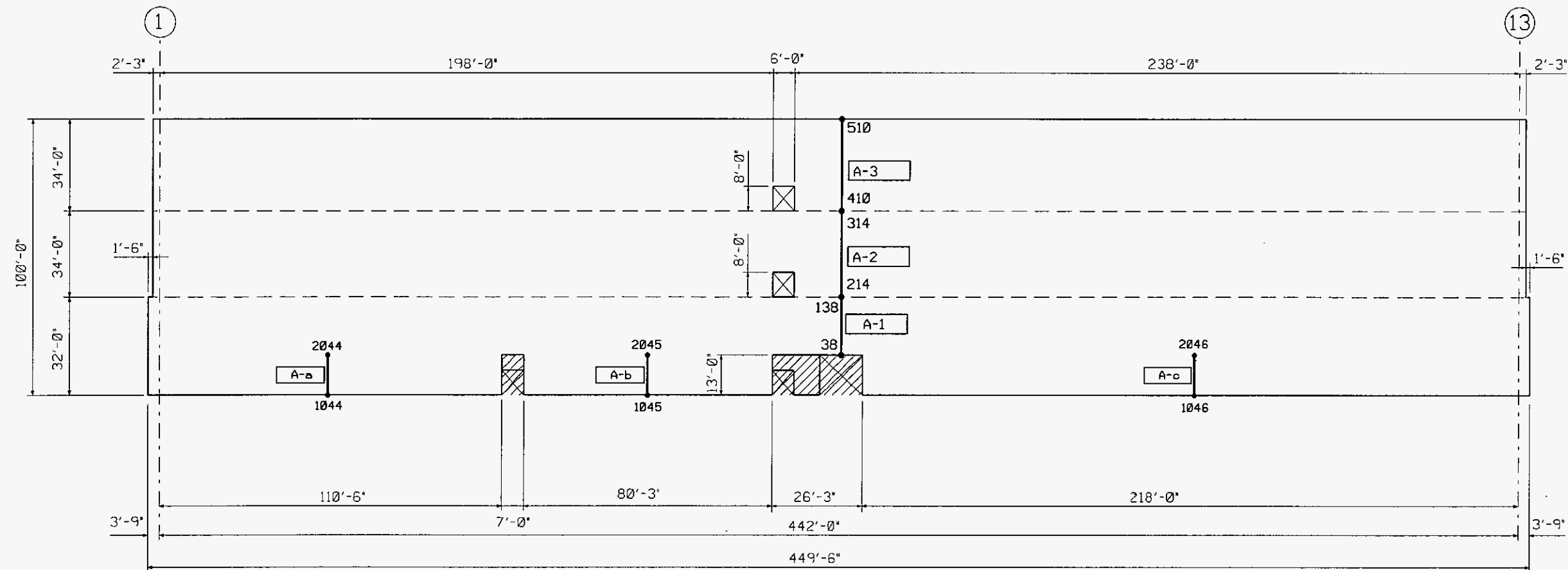


Wall Elevation @ Column Line 13.0

(Looking West)

N.T.S.

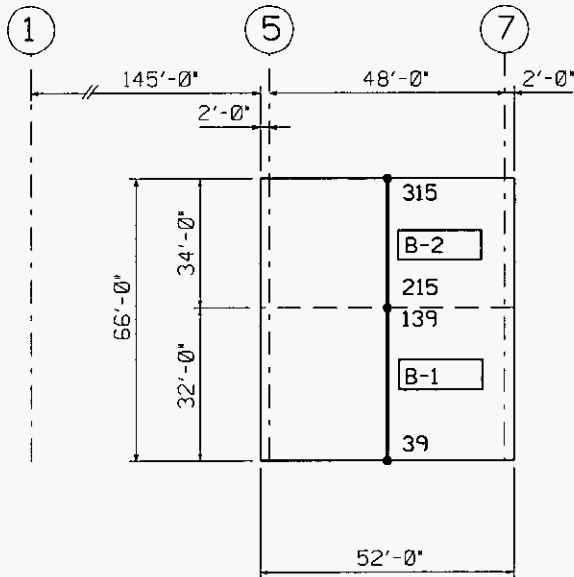




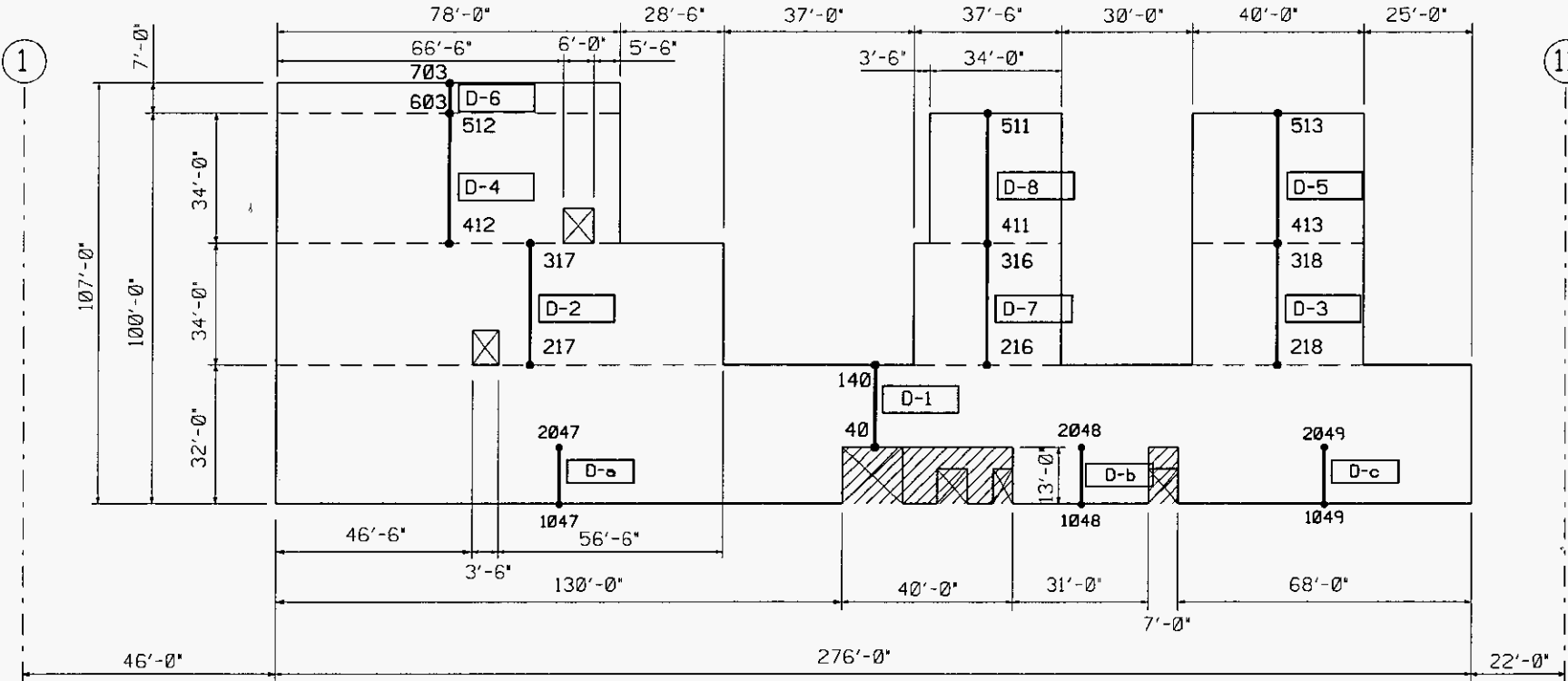
Wall Elevation @ Column Line A.0  
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N.T.S.

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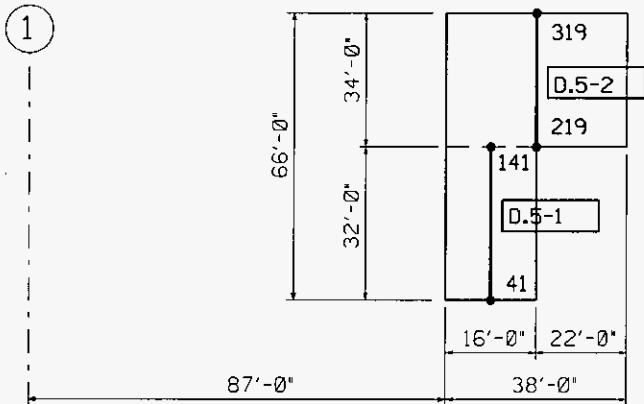
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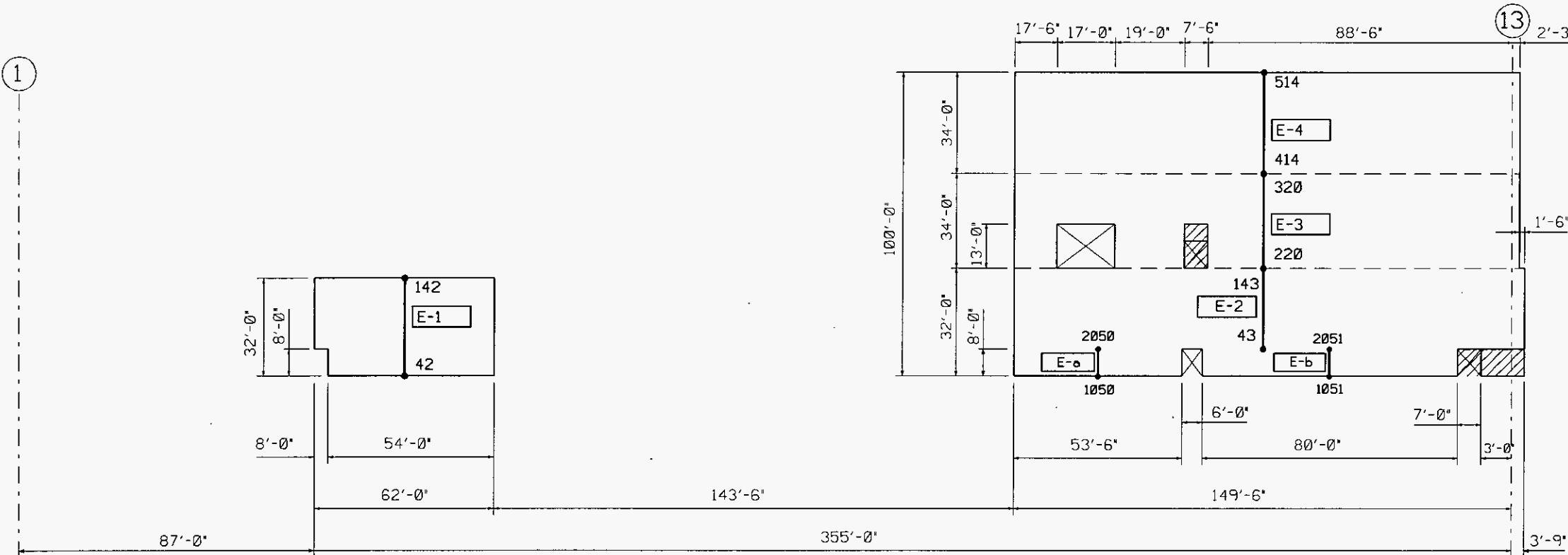
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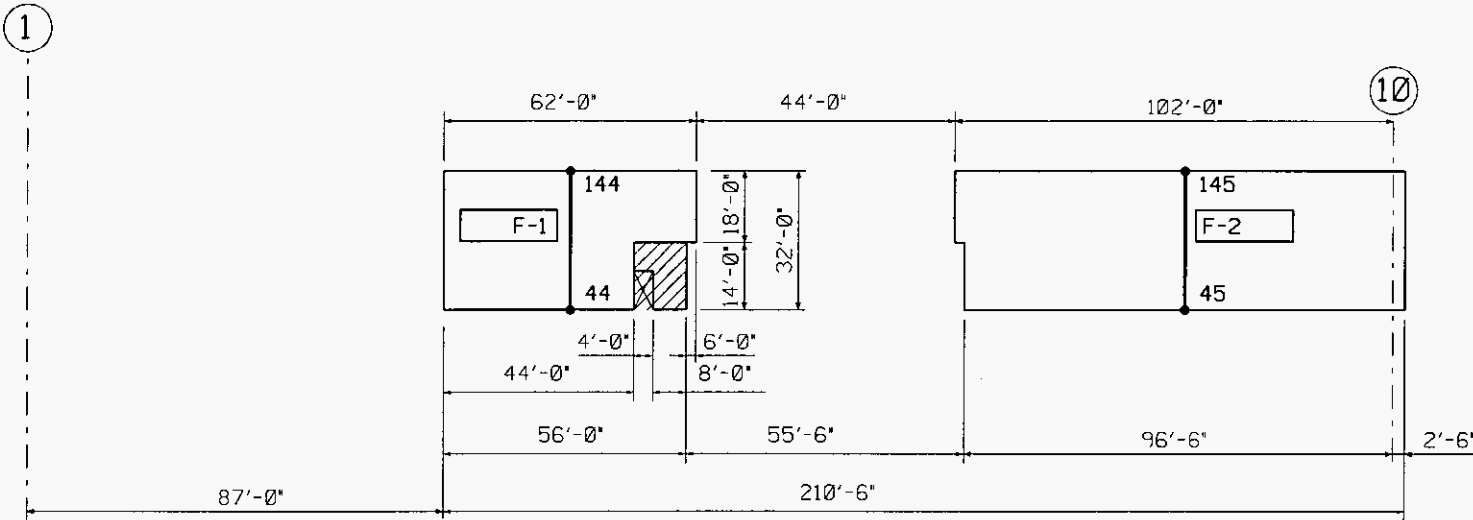
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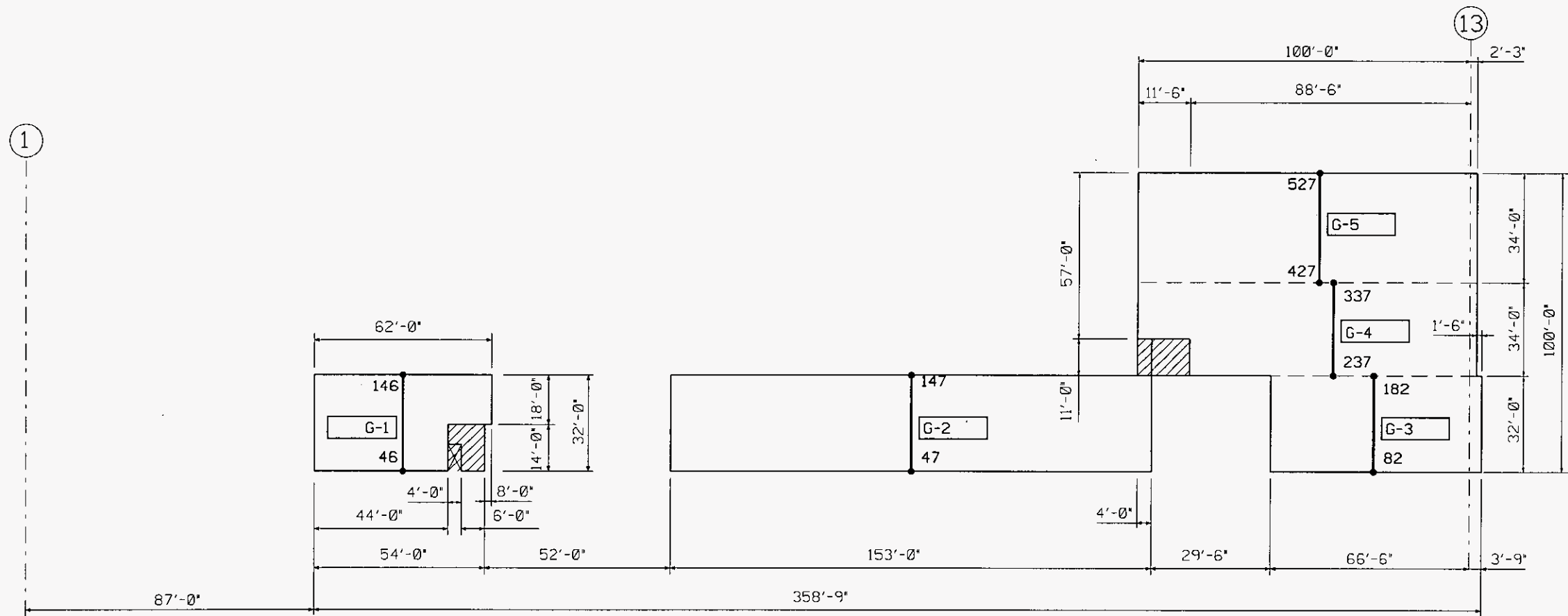
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N.T.S.



Wall Elevation @ Column Line E.0  
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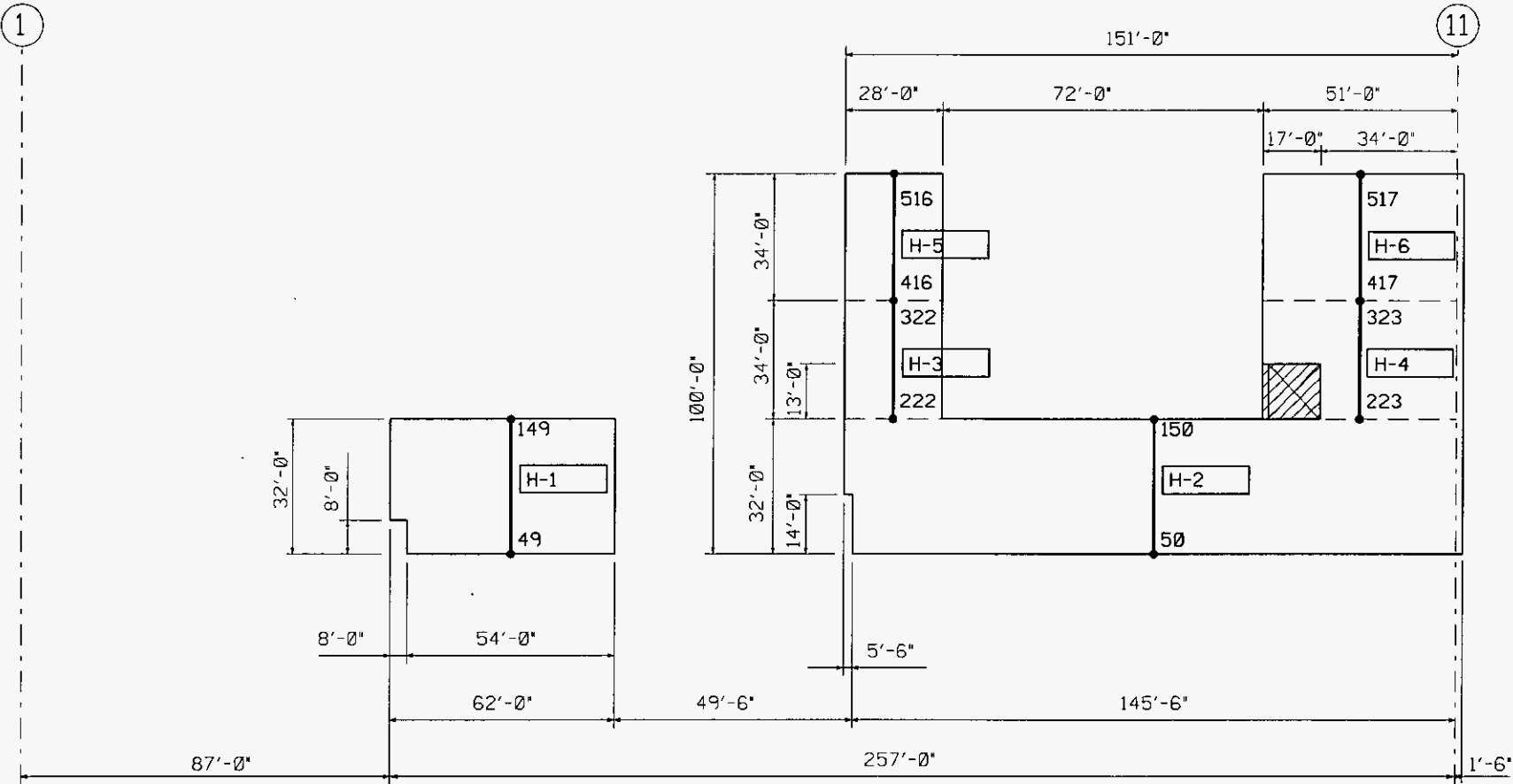
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Wall Elevation @ Column Line G.0  
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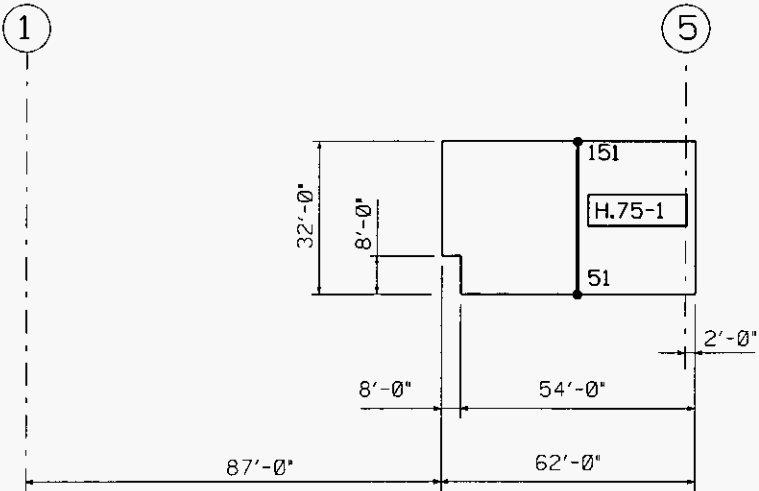
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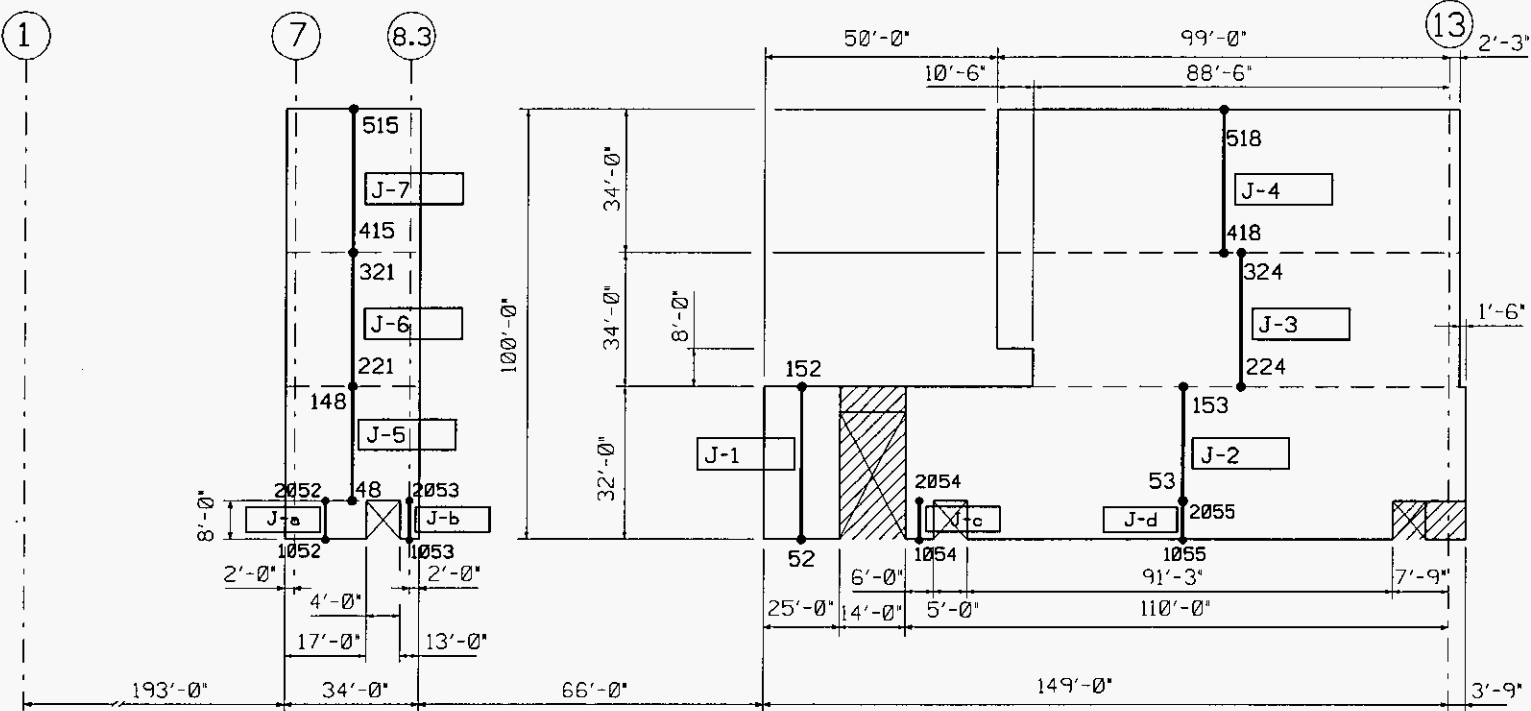
Wall Elevation @ Column Line H.0  
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N.T.S.

• ALL DIMENSIONS ARE +/- SIX INCHES

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Wall Elevation @ Column Line H.75  
(Looking North)  
N.T.S.

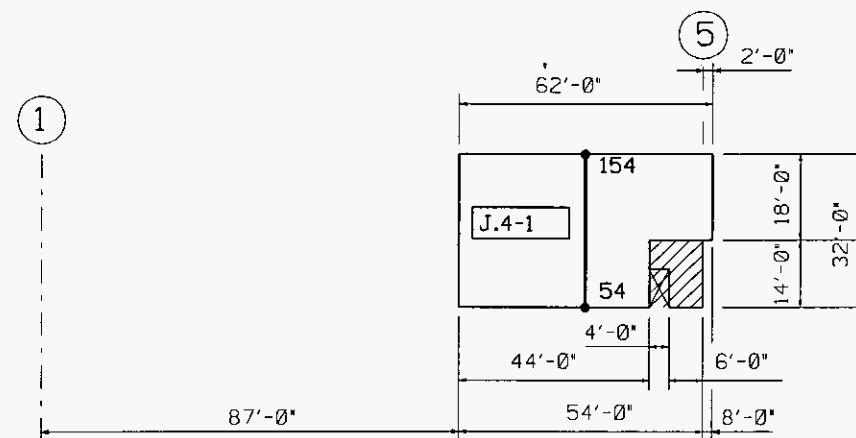


Wall Elevation @ Column Line J.0  
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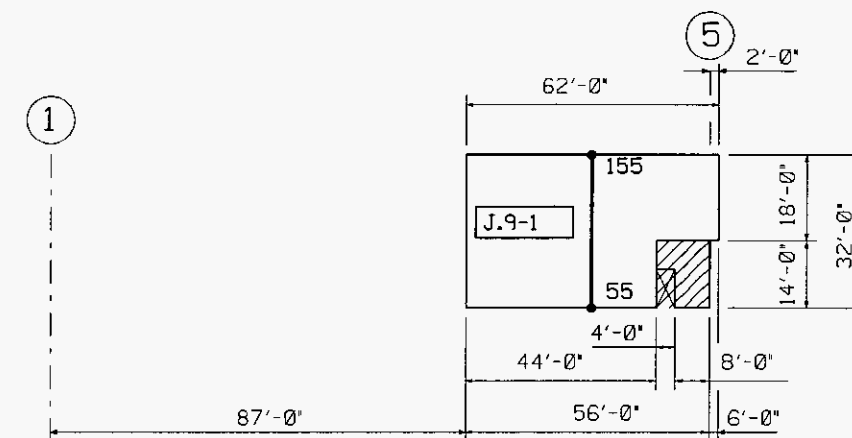


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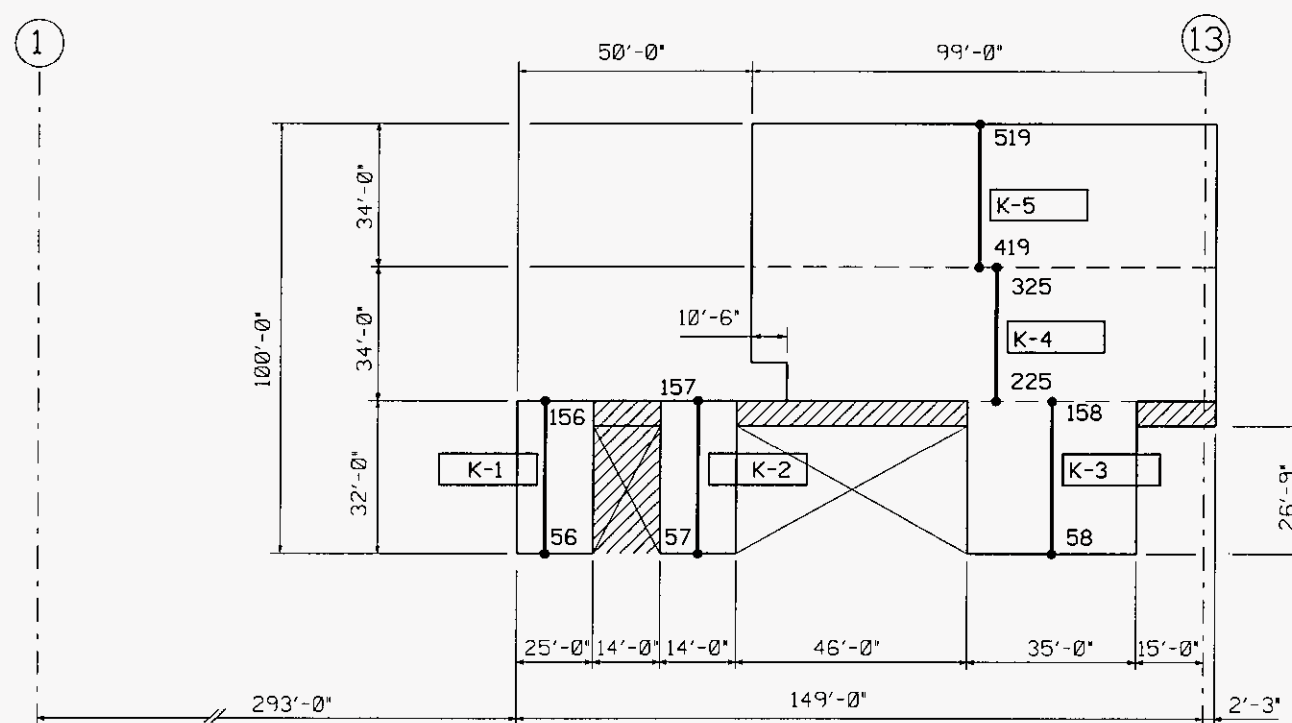
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N.T.S.



Wall Elevation @ Column Line J.9  
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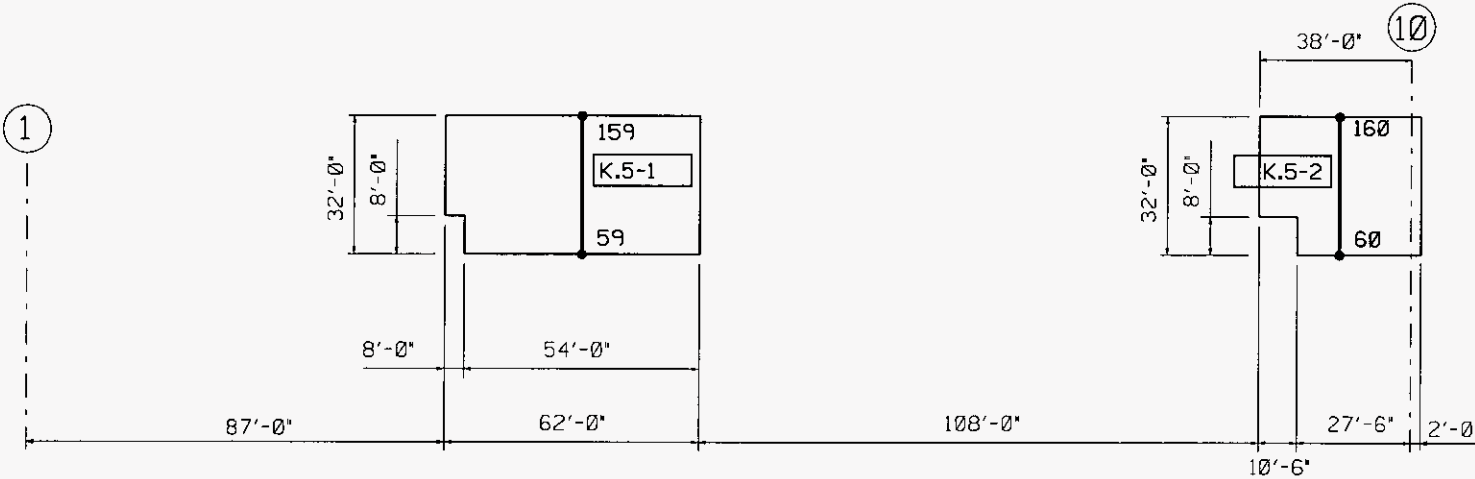
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Wall Elevation @ Column Line K.0  
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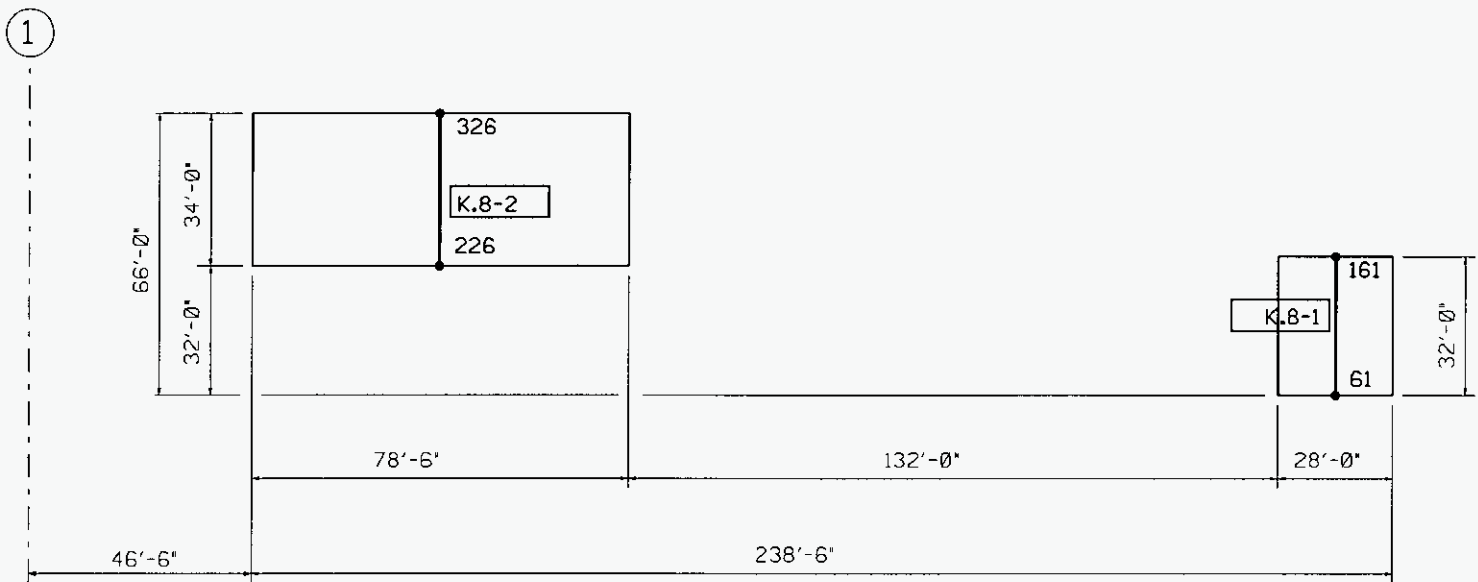
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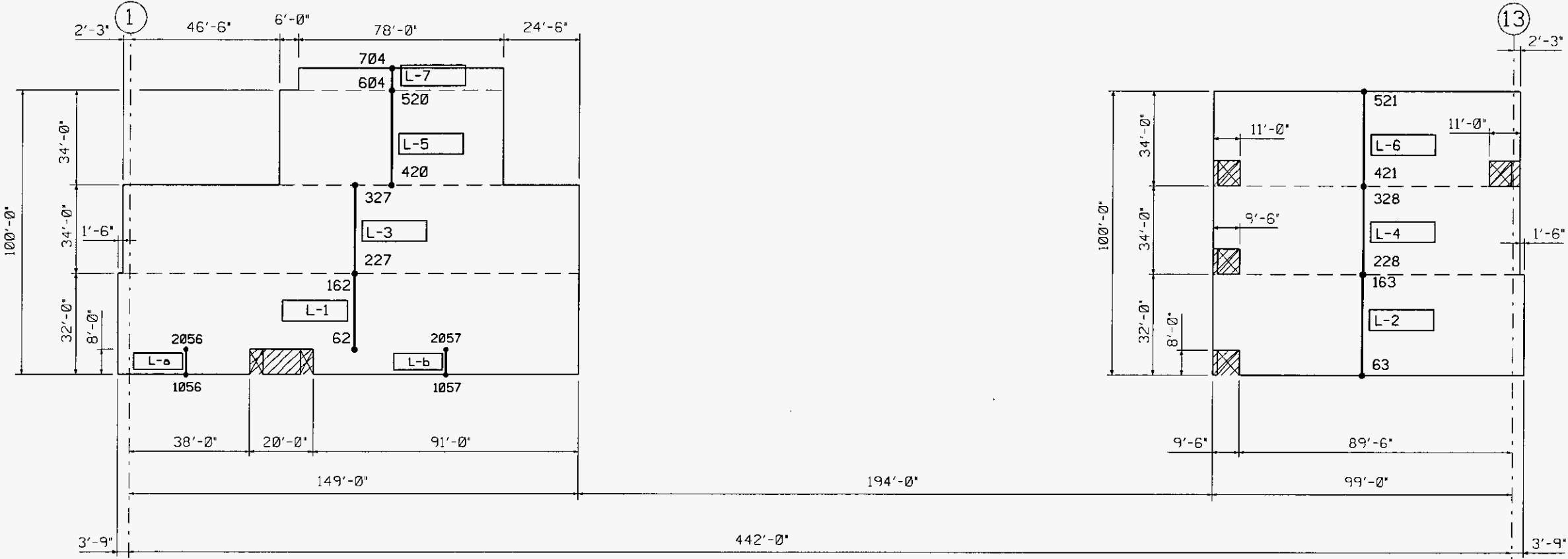
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• ALL DIMENSIONS ARE +/- SIX INCHES



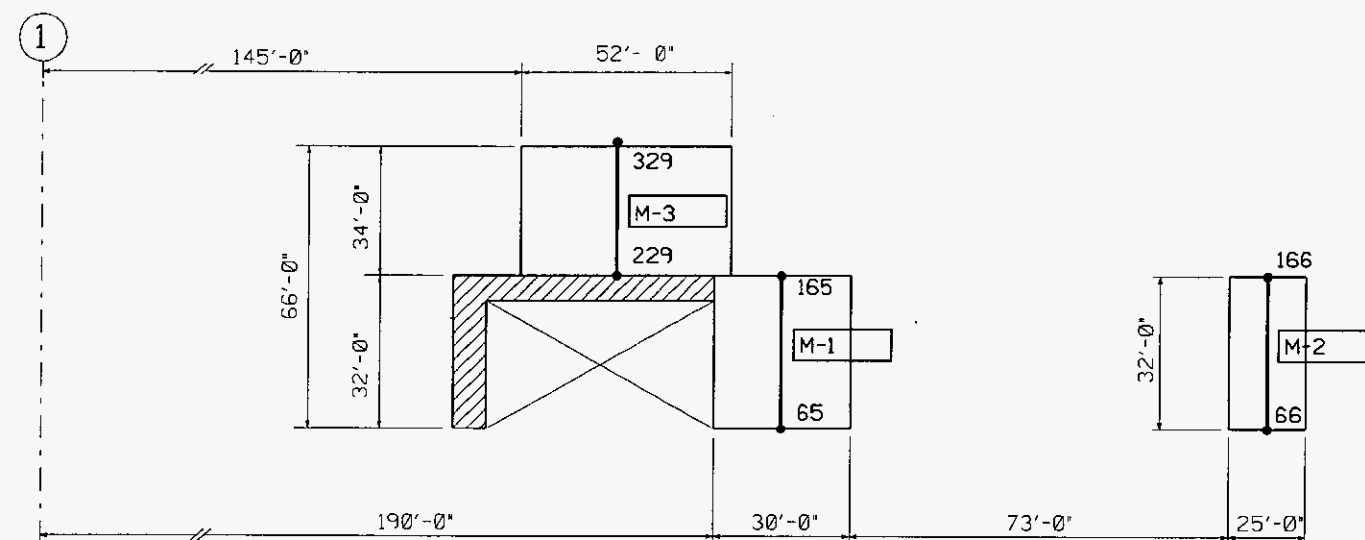
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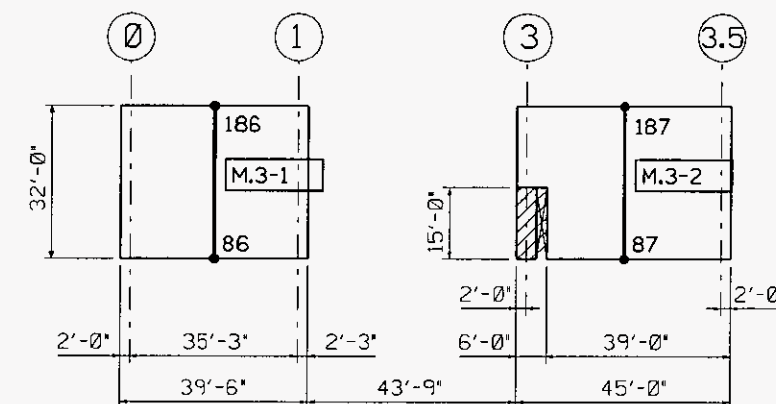
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• ALL DIMENSIONS ARE +/- SIX INCHES



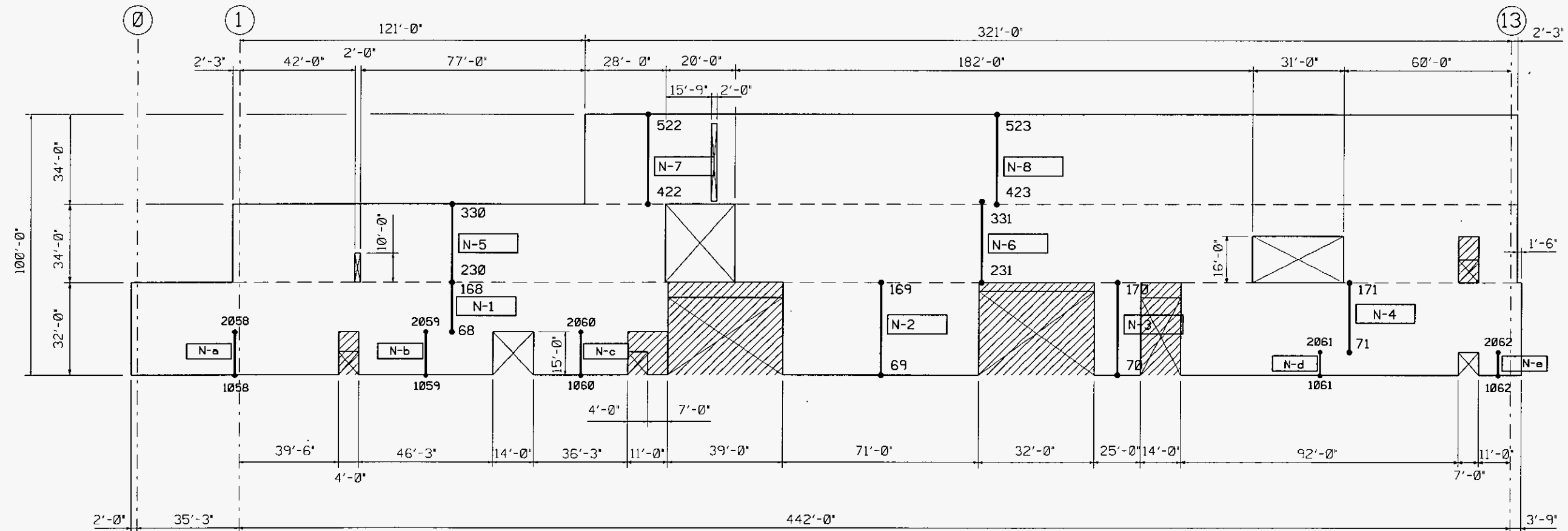
Wall Elevation @ Column Line M.0  
(Looking North)  
N.T.S.



Wall Elevation @ Column Line M.3  
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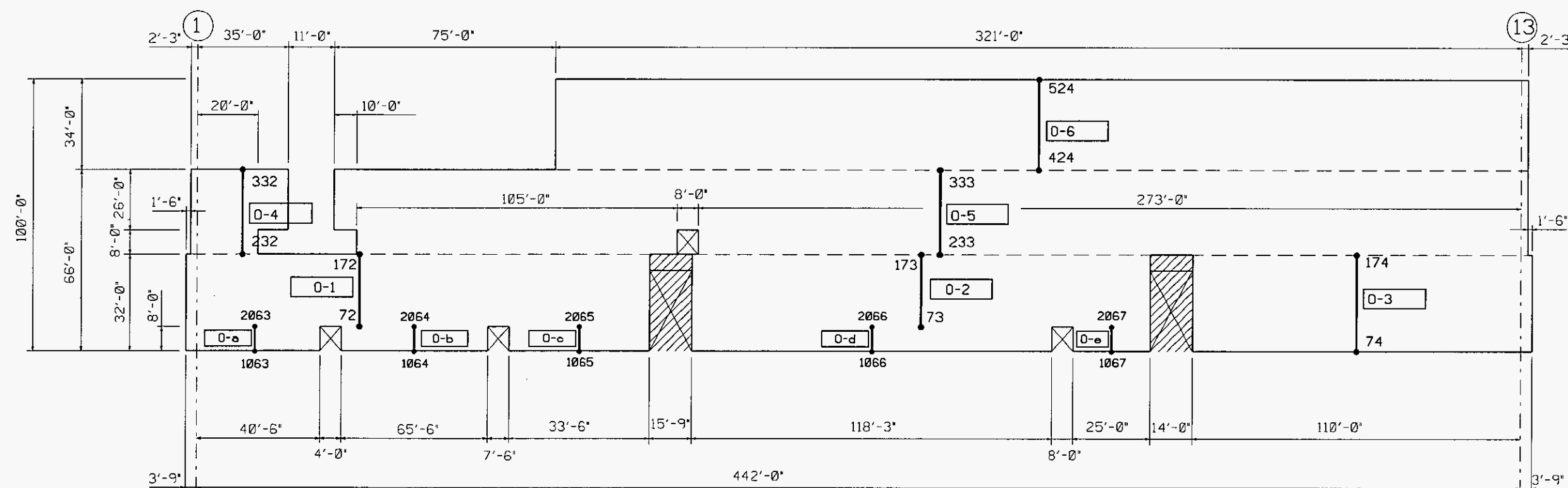
• ALL DIMENSIONS ARE +/- SIX INCHES



Wall Elevation @ Column Line N.0  
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N.T.S.

Document Identifier: 110-SYC-SY00-00300-000-00A  
 Title: Dry Transfer Facility Seismic Analysis

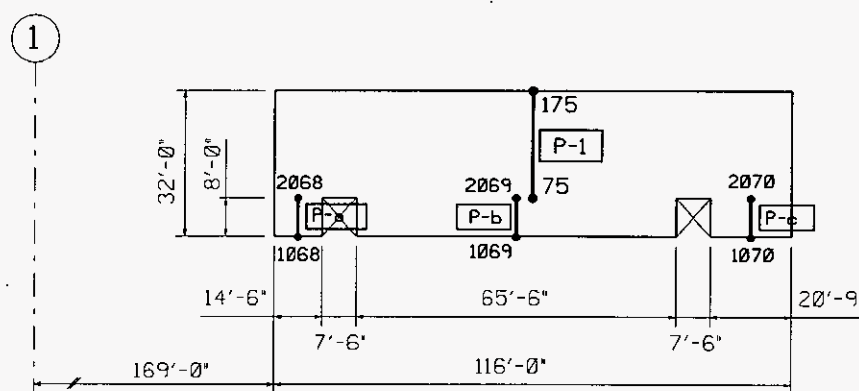
• ALL DIMENSIONS ARE +/- SIX INCHES



Wall Elevation @ Column Line 0.0  
 (Looking North)  
 N.T.S.



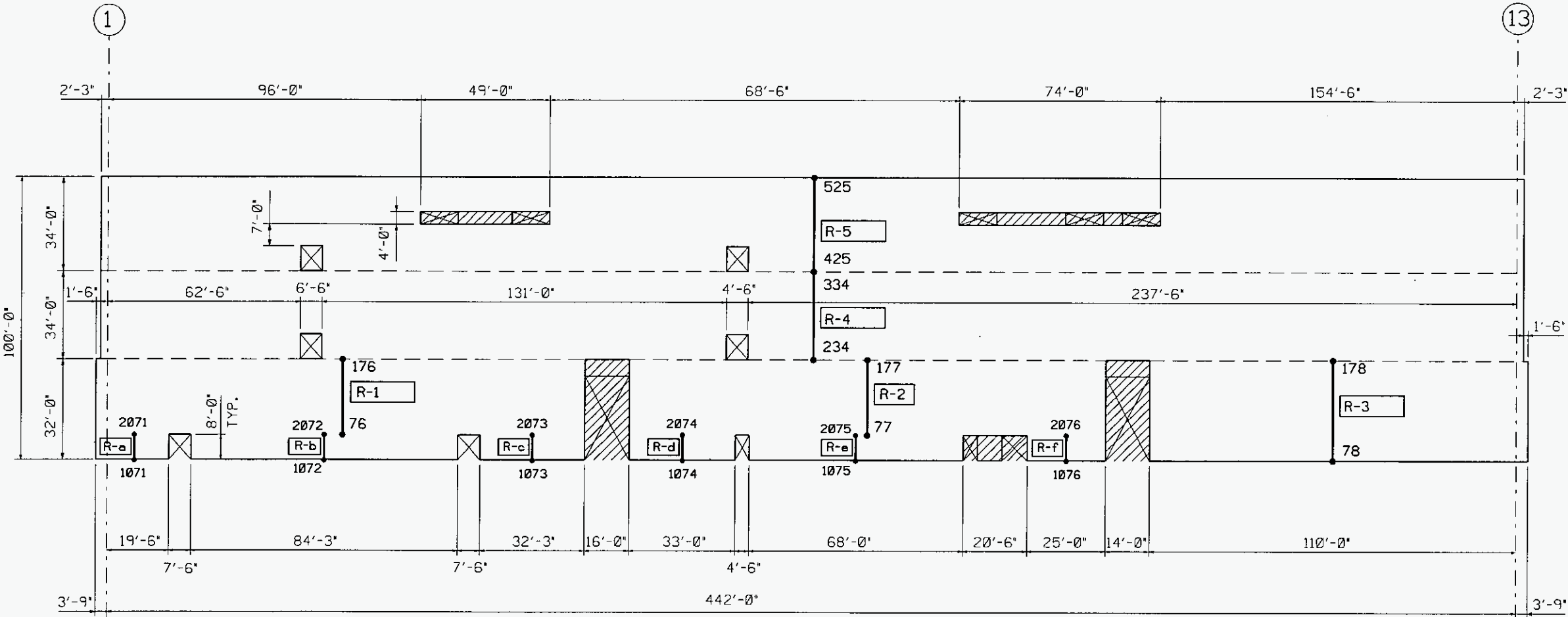
\* ALL DIMENSIONS ARE +/- SIX INCHES



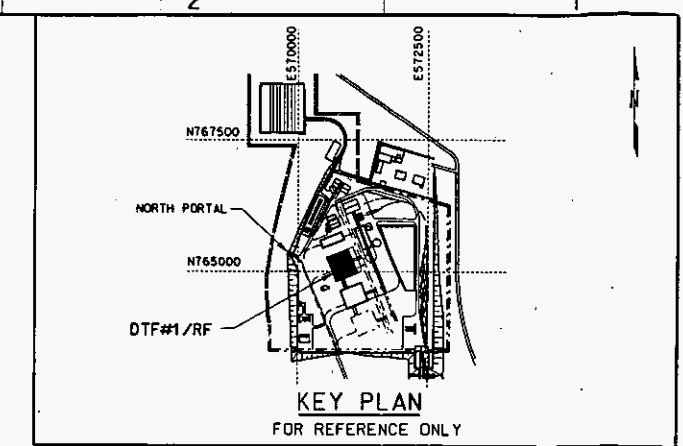
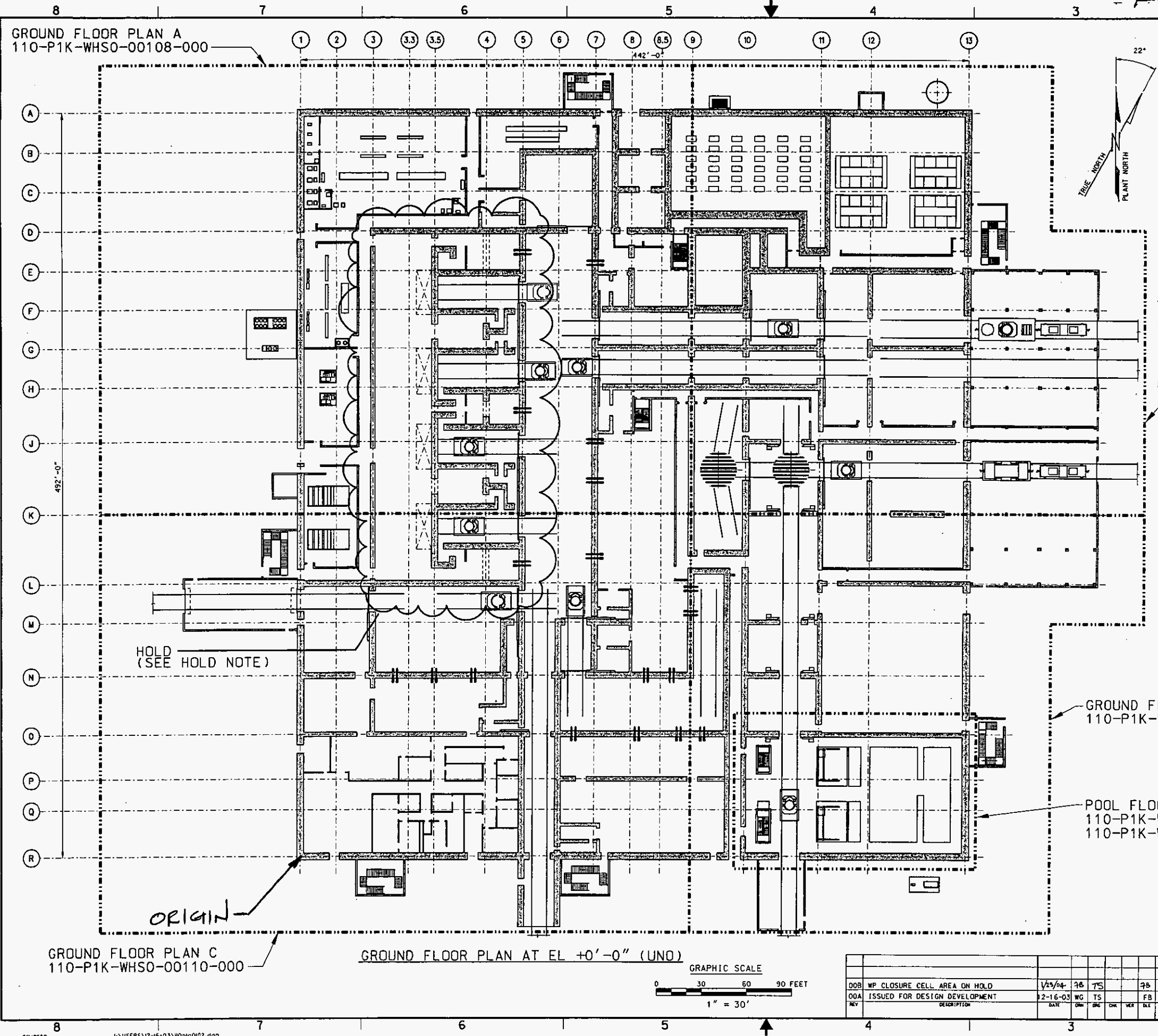
Wall Elevation @ Column Line P.0  
(Looking North)  
N.T.S.

Document Identifier: 110-SYC-SY00-00300-000-00A Title: Dry Transfer Facility Seismic Analysis

• ALL DIMENSIONS ARE +/- SIX INCHES



Wall Elevation @ Column Line R.0  
(Looking North)  
N.T.S.



**NOTES:**

1. FOR DRAWING INDEX, LEGEND & GENERAL NOTES SEE 110-P1X-WH50-00101-000.
2. ALL PERIMETER CONCRETE WALLS ARE 4'-6" THICK. ALL INTERIOR CONCRETE WALLS ARE 4'-0" UNLESS NOTED OTHERWISE (UND).

DI: 110-SYL-SY00-00300-000-00A  
TITLE: DRY TRANSFER FACILITY  
SEISMIC ANALYSIS

GROUND FLOOR PLAN B  
110-P1K-WHSO-00109-000

HOLD NOTE

1. ON HOLD FOR RESOLUTION FOR INNEL OA ISSUE

GROUND FLOOR PLAN D  
110-P1K-WHSO-00111-000

POOL FLOOR PLANS  
110-P1K-WHSO-00111-000  
110-P1K-WHSO-00124-000

THIS DRAWING IS PRELIMINARY AND NOT  
INTENDED FOR CONSTRUCTION. PROCUREMENT  
OR FABRICATION.

APPROVALS		DATE/TIME	<b>U.S. DEPARTMENT OF ENERGY</b> Office of Remediation Development (ORD) <b>RECEIVED</b>	
DRAWN BY: <b>FB FOR</b> W GUE COORDINATOR: T SAUER CHECKER:	<b>FB 1/23/04</b>  <b>T5 1/23/04</b>	Responsible for Management and Operation of the Office of Remedial Action and Waste Management Program <b>DRY TRANSFER FACILITY #1</b> <b>/REMEDATION FACILITY</b> <b>GENERAL ARRANGEMENT</b> <b>GROUND FLOOR KEY PLAN</b>		
VERIFICATION			DOCUMENT IDENTIFICATION SIZE: <b>D 1" = 30' - 0"</b> SCALE: <b>1" = 30' - 0"</b> SAFETY CATEGORY: <b>N/A</b>	
DESIGN LEAD ENGINEER <b>F. BASAMANOWICZ</b> QUALITY ENGINEERING REP: <b>PRZECYK ENGINEER</b> <b>L. ANDERSEN</b>		<b>FB 1/23/04</b>  <b>FB 1/23/04</b>	SHEET <b>110P-1K-WH50-00102-000-008</b> CAB FILENAME: <b>110p1a0102.dgn</b> SHEET: <b>2</b>	